

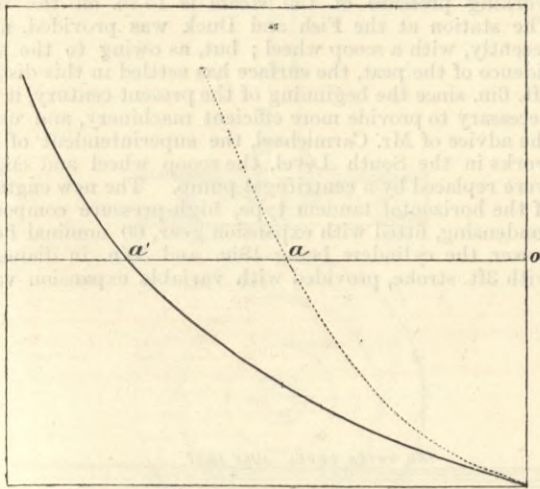
ELASTIC EXTENSION: A SPECIES OF MOTION.

By ROBERT HUDSON GRAHAM.

(Concluded from page 146.)

(8) *Assaying the Curve.*—The shape of a given curve, such as *a o*, Fig. 3, may be distorted by changing the fundamental scale of one of the ordinates, according to which it has been drawn. Supposing, for example, we double the horizontal scale of loads by simply doubling the length representing a given load; then it is clear that any point *a* upon the original curve is launched forward to *a'*, where its abscissa is doubled, whilst its ordinate remains the same. In this way the whole curve is projected from the dotted line to the black, as shown upon the figure.

Fig. 4



If, therefore, the original curve were of a particular nature, when plotted to a given scale or ratio of ordinates, it would at once lose cast by plotting the series of loads upon an exaggerated scale. The distorted form would, however, be derived from the original curve by projection in a constant ratio; and the original curve would be mathematically discoverable from the given projection.

In assaying any extension curve for cissoidicity it is advisable first to apply the ordinary cissoid test as shown in Fig. 2; that is, take the origin *O* at the limit of elasticity upon the curve, where it begins to break away from the straight line; describe the range-circle upon the distance *O l* contained between the limit *O* and the infinite ordinate to the curve at *l*; divide the range into any number of equal parts, and, using the centre *O* as a focus, draw the series of rays *O 1*, *O 2*, *O 3*, *O 4*, . . . meeting the series of ordinates from *1'*, *2'*, *3'*, *4'* . . . in *1''*, *2''*, *3''*, *4''* . . . all points upon the required cissoid. If the curve so constructed coincide with the extension curve, there is no scalar distortion. Should, however, the artificial curve vary much from the extension curve, it is necessary to ascertain whether this divergence is due to scalar distortion or to causes altogether independent of scale. If the variation arise merely from scalar effects, the primitive cissoid can be derived from its given projection according to some constant mathematical law. Now the general equation to the cissoid of extension is § 4.

$$y^2 = \frac{t^3}{2r - t};$$

if this curve be distorted by enlarging the scale of time and loads and keeping the scale of extensions constant, the new ordinate *y'* will equal *y*, the old ordinate, and the new abscissa *t'* will bear a constant ratio to *t*, the old abscissa of any given point. Let this ratio $\frac{t'}{t} = n$;

then, in order to return to the old equation, we must multiply all abscissæ *t'* of the projected form by the coefficient $\frac{1}{n}$, leaving the ordinates constant. Hence

we can retain the primitive equation to the curve, provided that all abscissæ taken from the projected curve be multiplied by the coefficient $\frac{1}{n}$; thus

$$y^2 = \frac{\left(\frac{t'}{n}\right)^3}{2r - \frac{t'}{n}} \dots \dots (1)$$

This equation contains two unknown quantities, the coefficient *n* and *2r*, the range of the original curve. In order to determine these two quantities, we must establish two equations by taking two values of *y* corresponding to two values of *t* from the given projection of the extension curve. Thus, for example, in Fig. 5 we have *y*=6, when *t*=12; and *y*=16, when *t*=19; hence, upon substitution and making $x = \frac{t'}{n}$, we obtain the two equations

$$(6)^2 = \frac{(12x)^3}{2r - 12x} \text{ and } (16)^2 = \frac{(19x)^3}{2r - 19x}$$

by the first of which the range

$$2r = 48x^3 + 12x, \dots \dots (2)$$

and substituting in the second this value of *2r* in terms of *x*,

$$\frac{6859x^3}{48x^3 - 7x} = 256. \dots \dots (3)$$

Dividing the numerator and denominator of this fraction

¹ The first part of this paper, excluding Sec. 7, was finished in January of this year, and read in the following month by an eminent Cambridge, as well as by an eminent Glasgow, professor.

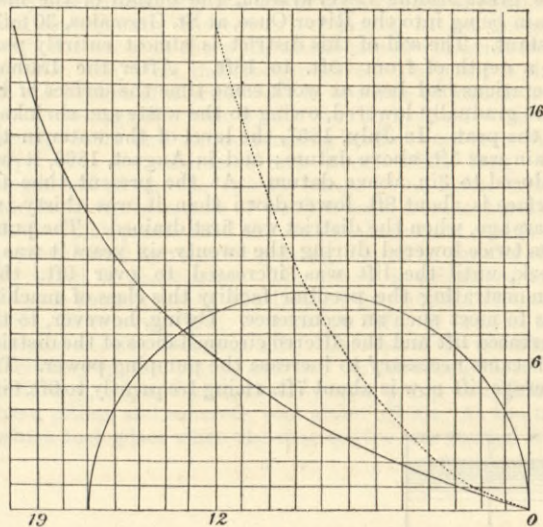
by *x*, the common factor, and solving, we find that very approximately the coefficient of distortion

$$x = 0.575;$$

and, thence, by substituting this value of *x* in Equation (2), the range, $2r = 17$.

Constructing the cissoid curve upon this range, as shown in Fig 5, it will be found that the abscissæ of all points upon the extension curve, which has been distorted by

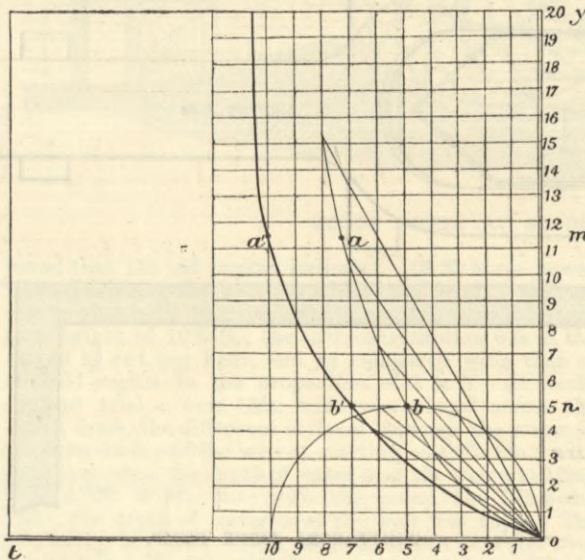
Fig. 5



adopting an exaggerated scale of loads, bear the constant ratio of $\frac{1}{x}$ to the abscissæ of corresponding points upon the primitive cissoid.

I have applied this kind of test to a fairly large number of extension curves, and have proved them in all cases, without exception, to be either primitive cissoids or projections of primitive cissoids. The dark line of Fig. 5 is the exact *fac simile* of a Wicksteed curve; so also is the dark line in Fig. 6, the data and results of the assay being given below the figure in the second case. I am indebted to Mr. J. Wicksteed, of Messrs. Buckton and Co., Leeds, for a copy of these curves. In everything connected with accurate experiment upon elasticity and its autographic diagrammatic expression, Wicksteed has taken a prominent lead.

Fig. 6



Wicksteed curves, new series of.—Copper bar turned to 1 square inch section. $d t = 1$ ton = 8 seconds = $\frac{1}{75}$ of an inch. Rupture at 10.8 tons from limit of elasticity at *o*. Extension, 45 per cent. of original length. Coefficient of distortion = $\frac{m a}{m a'} = \frac{n b}{n b'} = 0.7$. Curve *o b a* = primitive cissoid. Curve *o b' a'* = projection of primitive cissoid through the angle whose cosine is 0.7. Range = 10, diameter of circle of primitive curve.

It need not be remarked that the values $\frac{dy}{dt}$, $\frac{d^2y}{dt^2}$ are the same, whether taken from the primitive or derived forms; because, although *dy* may be smaller when expressed in terms of an augmented unit of scale *dt*, the number of these augmented *dt* to the current inch is also smaller in the same degree. In other words, the velocity of extension in any particular test must necessarily be the same, no matter what may be the scale of its representation upon paper. The foregoing conclusions appear at present in the garb of a particular induction, founded upon a large number of cases of bar, as distinguished from wire, tests. Whether it may be safe and justifiable to generalise this induction, so as to include all curves of every origin and species, is a question upon which it might be unwise to dogmatise. Nevertheless, it would seem that most extension-curves are so closely allied to cissoids as to perfectly tolerate the application of the rules and graphic processes developed in the preceding articles. But it must be carefully borne in mind that in cases where the curve proves to be a projection of a cissoid, the graphic method of determining the velocity of extension, the elastic acceleration, and the rest is applicable only to the primitive curve, which can be easily discovered by the method above explained. In choosing the two values of *y* and *t'* in the curve-projection of the cissoid as given by the test, in order to establish the two equations necessary to determine the unknowns *n* and *2r*, it is well to select those portions of

the curve which stand well out and clear of the focus where the two curves tend to blend and coalesce, and where consequently the corresponding values of the two ordinates are not well-defined.

(9) *Recapitulation.*—In conclusion, the author begs to state his belief that the novel treatment of elastic extension, set forth in this paper, will be found to comprehend and satisfactorily explain the usual phenomena attendant upon ordinary metallic tests, excluding cases of exceptional character. The chief motives which prompted the author to write the paper were a desire to submit his researches to the judgment of other minds, to stimulate discussion upon the subject, and to draw attention to what appeared to him the simplicity and elegance of the elastic graphic expression for the velocity of extension, the acceleration, the new feature of elastic excess, and the increment of extension due to the vibratory effect of the load.

With respect to the work of other minds in this special field of thought, no attempt has hitherto been made to bring elastic extension under ordinary dynamic laws. There is, indeed, a paper by Sir W. Thomson on "Elasticity, a Mode of Motion," read before the Royal Institution, which deals with the subject from a physical, or rather metaphysical, point of view. It would seem to be a proof that elasticity, like heat, is in ultimate analysis an aspect of motion. But engineers, even those who are of a pronounced scientific bent, will take leave of the great master of physics whenever he passes beyond that clear line dividing the territory of practical mathematics from the vague spaces of metaphysical speculation.

With regard to the variation of rate at which the load is added, and its effect upon the ultimate strength of metallic wire, a series of experiments of a more or less rigorous nature was carried out in the Glasgow University Laboratory, and an account of them published in the "Proceedings of the Royal Society"—vol. xxix., p. 221. The deduction based upon these experiments, as given in Mr. J. T. Bottomley's paper, was that "wire broken rapidly receives an elongation of over 25 per cent. on the average; whilst the same wire broken slowly is elongated only by about 7 per cent." The length of wire employed was 16ft., and its diameter .036in. In one case, when loaded at the rate of $\frac{1}{2}$ lb. per minute, the specimen broke under a total load of 45 lb., and a total extension of 25 per cent. At another time, when loaded at the rate of 1 lb. every three minutes, it finally broke under a load of 45½ lb., and an elastic extension of 29.6 per cent. In a third instance, when loaded at the rate of 1 lb. every twenty-four hours, it broke under a load of 48 lb., with an elongation of 7.58 per cent. Lastly, a bright annealed specimen of the same dimensions, when loaded at the rate of 1 lb. every twenty-four hours, broke under a load of 47 lb., and an extension of 6.92 per cent. The same specimen, loaded at the rate of $\frac{1}{2}$ lb. per twenty-four hours—which, by the way, is not the same as 1 lb. per forty-eight hours—broke, firstly, under a load of 47 lb., and an extension of 4.79 per cent.; and, secondly, under a load of 46½ lb. and an extension of 6 per cent. The rate of load was afterwards reduced so low as a shot per day; but, whilst greatly edified at the astonishing patience of the operator, engineers will be more particularly interested in swift than in slow rates of fracture. It will be seen that these experiments tend to confirm the theory that extension varies largely, whilst the ultimate breaking-strength varies but little, for different rates of load addition. Thus, whilst the rate diminished from $\frac{1}{2}$ lb. per minute to $\frac{1}{2}$ lb. per day, the ultimate extension decreased from 25 per cent. to about 7 per cent.; whereas, for the same variation of rate, the ultimate breaking-strength increased only by about 2 lb. It must, however, be carefully borne in mind that the analogy between intermittent loading of this nature and the continuous loading assumed in our investigation is far from being complete.

At a later date some experiments were undertaken by Mr. Herbert Tomlinson, towards the expenses of which the Government Research Fund contributed a sum of £4000. An account of these experiments will be found in a paper communicated by Professor W. G. Adams to the "Phil. Trans." of the Royal Society, 1883. There is, however, little to be found in them immediately bearing upon the question of time-tests. It is only stated in a general sort of way that "in the case of a wire which has suffered permanent extension, the extension decreases in proportion as the time between the loadings increases." This fact was also pointed out by Professor Ewing—"Proc." Roy. Soc., 1880, vol. xxx., page 510. The same phenomenon had, however, as we have seen, previously appeared in Mr. Bottomley's experiments; and, in fact, long before that time it had formed part of the engineering faith, and had been incorporated in the principles of bridge construction under the form of varying co-efficients for live and dead loads.

In case absolute accuracy were required in ascertaining the nature of the extension curve, it would, of course, be necessary to employ the method of least squares. But we need scarcely remark that, owing to defects in the tracing gear, and to other mechanical imperfections, the coloured pencil does not trace a perfectly continuous curve, and therefore we are free to consider all the tests and results in the light of tolerable approximations to the truth. All theories based upon experimental data are necessarily imperfect in their origin, which fact enables us to dispense with excessive refinement in the practical operations to which they give rise.

The elastic excess *z*, is the strain measuring the loss of tension, $\frac{E \varpi z}{l}$, due to acceleration and other accidental causes. Its value is determined independently of sign, and its nature is essentially negative. Thus, as explained in Art. 3, the actual tension, $\frac{E \varpi y^1}{l}$, is always less than the static extension, $\frac{E \varpi y_0}{l}$. Taking account of the contraction of area from ϖ to ϖ^1 , this tensional loss may be expressed by $E(y_0 \varpi - \varpi^1 y^1) \div l$.

THE DRAINAGE OF FENS AND LOW LANDS BY STEAM POWER.

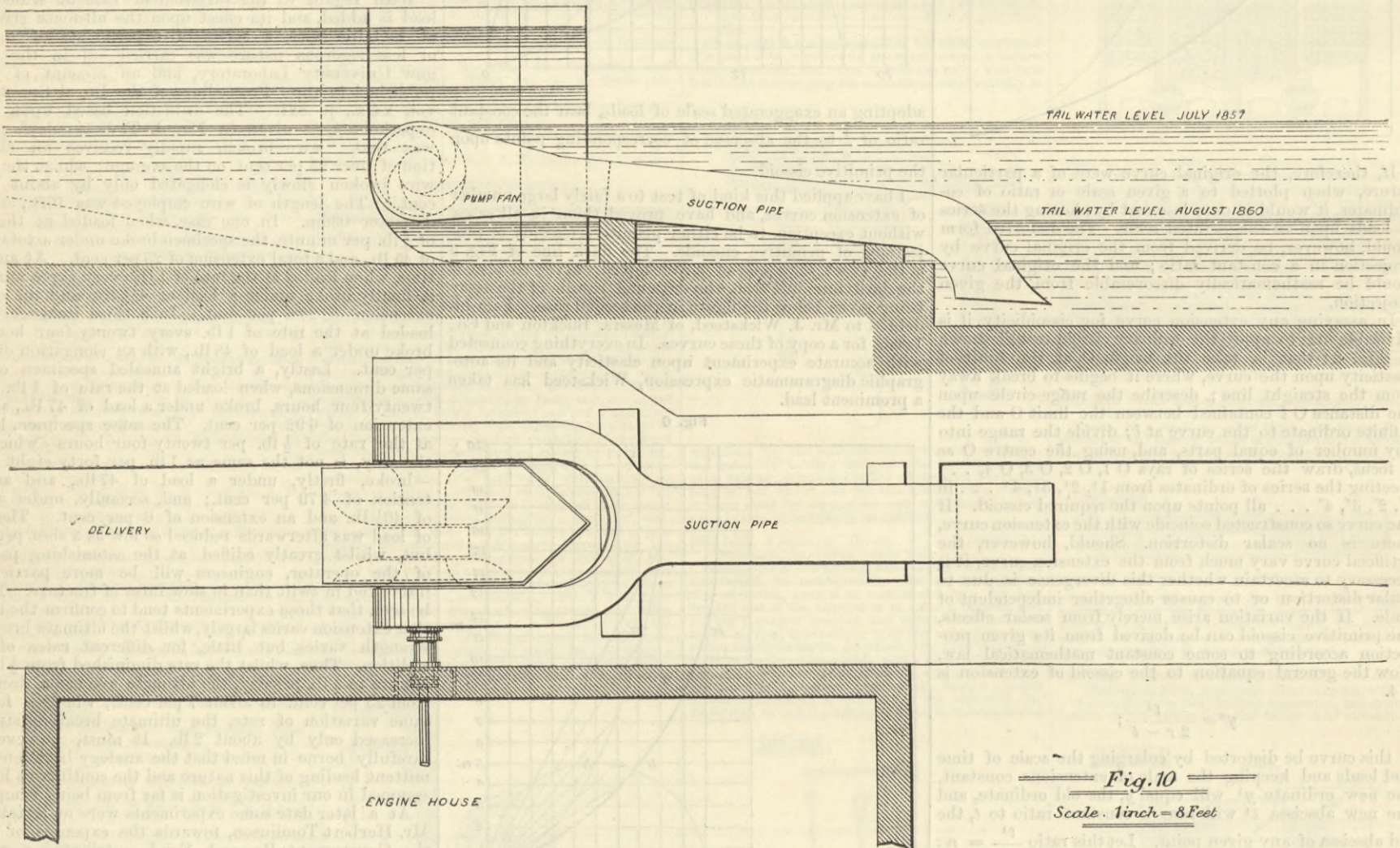
By W. H. WHEELER, M. INST. C.E.

No. XI.

The Ten Mile Station.—The scoop wheel at this station is 43ft. 8in. diameter, having been increased 20in. from the original dimension by lengthening the scoops. There are fifty scoops, 7ft. 6in. radial length by 3ft. wide. The average dip of the scoops is 3ft.; the greatest, 5ft. 6in.; and the lift 11ft. average, and 14ft. maximum. This wheel lifts the water into the Ten Mile river, which is not tidal, the tide being shut out by sluice doors at Denver Sluice. There is, however, a considerable rise in the river during tide time. These scoops drip from the radial line at an angle of 38 deg., being tangent to a circle of 18ft. diameter, and on an average head and dip of 14ft.—11ft. head and 3ft. dip—enter the water at an angle of 34 deg., and leave it at an angle of 72 deg. The wheel makes $4\frac{1}{2}$ revolutions a minute. When working to its full extent, the wheel is capable of discharging 213 tons per minute. This wheel has been provided with a movable breast, as at the other station. The engine for driving the wheel is similar in character to that at the Hundred Foot Station, and was altered and adapted for working with a higher pressure of steam in a manner similar to the other. The cost of alterations at the two stations was over £6000. The estimated capacity of the two wheels at the maximum dip is 410 tons per minute. This is equal to a discharge of water due to a continuous

was of 24 nominal horse power, driving a double inlet horizontal spindle Appold centrifugal pump, 4ft. 6in. diameter, with an average velocity of 90 revolutions a minute, equal to 1431ft. per minute; the lift at that time being from 4ft. to 5ft. The pump was driven by a double-cylinder steam engine, with steam at 40 lb. pressure, and vacuum 13½ lb. It raised 15,000 gallons—67 tons—per minute to a height varying from 2ft. to 5ft. The total cost was £16,000, of which about £2000 was for the machinery. The general arrangement of the pumps is shown by the sketch, Fig. 10. The pump discharged into Bevil's river, a branch of the Nene, which forms a part of the great Middle Level system, the outfall of the main drain being into the River Ouse, at St. Germain's, 30 miles distant. The soil of this district is almost entirely peat, to a depth of from 15ft. to 18ft. After the drainage operations had been at work some time the surface of the land gradually lowered, owing to the waste and shrinkage of the peat. In July, 1857, the level of the water in the drain was 5ft. above datum; and in August, 1860, it was reduced to 3in. above datum. At the present time the surface is about 8ft. lower down than it was thirty-two years ago, when the district was first drained. The pump was twice lowered during the twenty-six years it was at work, until the lift was increased to over 9ft., thus demonstrating the peculiar facility this class of machine has to meet such an occurrence. Owing, however, to the increased lift and the altered circumstances of the district, it became necessary to increase the pumping power. The average lift now is about 7ft., rising frequently to 9ft. 6in.,

junction with the Ouse; the other on the north, discharging into the Little Ouse, about two miles above Brandon Creek Bridge. The main drains between the two stations are in connection, so that the water can run to either station. These pumping stations are about eight and fifteen miles respectively above Denver Sluice, where are self-acting doors, which shut against the tide at the time of high water. The lift at the north station is rather the highest, the average of the two stations being about 10ft. 6in., rising in heavy floods to 16ft. The north station consists of a scoop wheel 34ft. 6in. in diameter, with scoops 4ft. 9in. long by 2ft. wide, motion being given by one engine of 40 nominal horse-power. The wheel is driven by a condensing engine of the old marine side-lever type, having the beam below the cylinder. The piston has 3ft. 6in. stroke, and makes 28 revolutions of the engine to 5½ of the wheel. The working pressure of the steam is 15 lb. on the inch. The station at the Fish and Duck was provided, until recently, with a scoop wheel; but, as owing to the subsidence of the peat, the surface has settled in this district 4ft. 6in. since the beginning of the present century, it was necessary to provide more efficient machinery, and under the advice of Mr. Carmichael, the superintendent of the works in the South Level, the scoop wheel and engine were replaced by a centrifugal pump. The new engine is of the horizontal tandem type, high-pressure compound condensing, fitted with expansion gear, 60 nominal horse power, the cylinders being 18in. and 30in. in diameter, with 3ft. stroke, provided with variable expansion valve



WHITTLESEA MERE PUMP.

daily fall of 0.17in. of rain. In the year 1883, which was a very wet season, the engines ran as follows:—

	Hundred Foot engine.	Ten Mile engine.
Total hours run	2288	2280
Coals consumed	691 tons	589
Average dip of the scoops	3.30 feet	3.08
Greatest dip of the scoops	5.33 feet	4.58
Average head	13.80	11.16
Greatest head	17.2	13.4

The estimated discharge, calculated with the average dip of the scoops given above, is 122.12 tons per minute lifted 13.80ft., equal to 114.40-horse power of water lifted, with a coal consumption of 5.99lb. per horse-power of water lifted for the Hundred Foot engine, and 128.55 tons lifted 11.16ft., equal to 97.38-horse power, with a coal consumption of 5.93 lb. per horse-power, for the Ten Mile Station. Taking the two wet years, 1881 and 1883—1882 being omitted, as during this time the machinery was under alteration—the cost of lifting the water was as follows:—Coals, £717; attendance and other expenses, £203. The area drained being taken at 35,000 acres, this gives 12.62d. per acre per annum for working expenses. The average height to which the water was lifted at the two stations being taken at 11½ft., gives 1.10d. per acre per foot of lift, or, for coals only, of 0.85d. per acre. Coals costing about 17s. per ton.

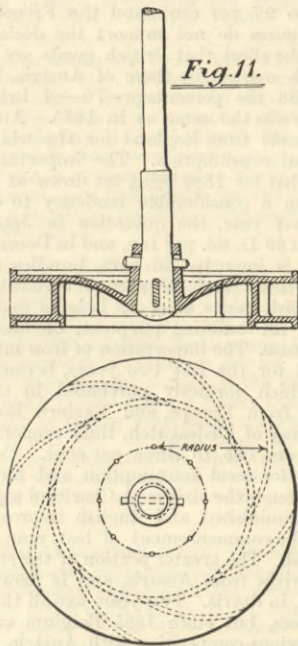
Whittlesea Mere.—This pumping station is in the Middle Level, in the county of Huntingdon, and contains about 6000 acres. The Mere originally was a large lake or morass, which produced nothing but reeds and wild fowl. This, with the surrounding fen, was embanked and drained by steam power by the proprietor, Mr. Wells, in 1851-52, being the first instance in this country where the centrifugal pump was applied to this purpose. The results obtained with the Appold pump at the trials of this machine at the Exhibition of 1851, demonstrating its suitability for the purpose. The engine then erected

and even higher in heavy floods. In 1877 the old engine and pump were removed, and the fan of the pump may now be seen at the Museum at South Kensington in almost perfect condition. Messrs. Easton and Anderson erected in their place a high-pressure compound condensing beam engine, with expansion gear, of 65 nominal horse-power, making about 36 revolutions a minute with 60 lb. steam. The boilers consist of one single flued and one double flued Cornish boilers. The pump, which is placed in a well outside the engine house, is driven by a double set of motions, the first set consisting of a tothing on the fly-wheel driving a pinion which actuates a horizontal shaft for driving a wheel geared into a bevil wheel on the vertical shaft of the pump. This is hung by an onion bearing to a cast iron frame bolted to the top of the pump well, which is formed with a wrought iron cylinder fixed in the centre of the sluice connecting the main drain with the river. This cylinder was used as a convenient mode under existing conditions of forming the pump well, and reduced the first cost by avoiding the necessity for building a brick well. This sluice is 12ft. wide on the inlet side and 6ft. on the delivery side. The fan is a single inlet fan of 6ft. diameter by 16in. deep, and is speeded to run up to 104 revolutions a minute when on a lift of 11ft. The quantity of water delivered is 96 tons per minute, or on a lift of 7ft. 6in., with a speed of 96 revolutions of pump, 155 tons per minute. The engine and boiler are contained in a brick building. The chimney shaft is 53ft. high and 3ft. diameter at the top inside. The cost of the machinery was approximately £3500, plus the value of the old machinery.

Burnt Fen, Norfolk.—This district is situated in the south level of the Bedford Level, and is entirely Fen land. The area drained by the pumps is 15,000 acres. There are two pumping stations, about four miles apart—one at the Fish and Duck, on the south side of the district, discharging into the river Lark, about three miles above its

working on the back of the high-pressure valve. Steam is provided by three Lancashire boilers, 25ft. long by 7ft. diameter; the working pressure being 65 lb. Only two of the boilers are in use at the same time. The engine makes 70 revolutions with steam at 65 lb. in the boiler, and cut off in the small cylinder at half of the stroke, the pump making at the same time 105 revolutions with a lift of 14ft. per minute, and delivering 120 tons. The case of the pump is 9ft. 6in. diameter, situated in a well immediately outside the wall of the engine house. This well is 9ft. 10in. in diameter; the diameter diminishing below the pump to 6ft. The outlet for the discharge is 9ft. 6in. above the centre of the pump, and is 5ft. 6in. high by 3ft. 6in. wide. The pump is driven by a bevil wheel geared into a bevil pinion on the crank-shaft, which is 11ft. long. The fan is single, made of gun-metal, 6ft. diameter by 12½in. deep at the periphery, with a short suction pipe attached to the case below the disc. The spindle is suspended by an onion bearing supported by a girder across the top of the cylinder of the pump well. When the pump is working it is found that little weight is carried by the onion bearing, as the disc is so arranged that the water entering it supports the moving parts. The pump was calculated to lift the following quantities:—121 tons at 9ft.; 115 tons at 10ft.; 109 tons at 11ft.; 104 tons at 12ft.; 100 tons at 13ft.; 96 tons at 14ft.; 92 tons at 15ft.; 89 tons at 16ft. These quantities were exceeded at the trials of the pump. The engine bed occupies a space of 30ft. by 5ft. 6in. The engine and pump were supplied by Messrs. Hathorn, Davey, and Co., of Leeds. The contract price, including the well and fixing in the old building, the makers taking the old engine, was £2700. A drawing showing the arrangement of the pump and engine will be found in THE ENGINEER, vol. lvi., February, 1884, and an enlarged view of the pump is now given in Fig. 11. Careful observations have recently been taken by Mr. Carmichael as to the con-

sumption of coals by this engine under ordinary working conditions, the quantity of water delivered being ascertained by measuring the quantity passing through the outlet drain. With a lift of 11ft. the quantity of water discharged was 120 tons per minute, with a consumption of three tons of Derbyshire coals in twelve hours. This is at the rate of 6½ lb. per horse-power of water lifted per minute. The quantity of oil used for lubricating is at the rate of one gallon in twelve hours. The consumption of coals in this district has varied during the last twenty years from about 250 tons to 1000 tons in a year according to the rainfall, the average cost for the

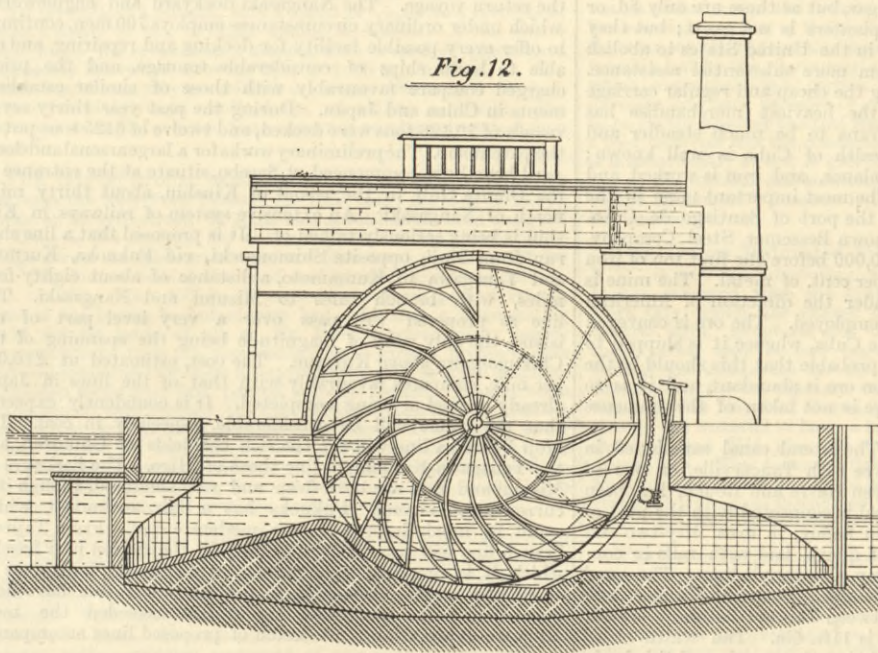


years 1881-83, coals being then about 15s. per ton, was, for coals, £674; attendance, oil, &c., £252; total, £926. Taking the average lift for both stations at 10½ft. this is equal to 1481d. per acre, or per acre per foot of lift, 1.42d.; or for coals only 1.02d. During this time both scoop wheels were in operation. The main drain, which brings the water to the pump, is 20ft. wide at the bottom, with slopes of 1½ to 1. The average depth of water when pumping is going on, varies at starting from 5ft. 6in. to 3ft. at leaving off; the surface inclination also varying from 2½in. per mile to 4in.

Prickwillow.—This pumping station is for the drainage of a large district in the South Level, being part of the Great Bedford Level, in the county of Cambridge. The taxable area of the district is about 11,000 acres, but the area of land actually drained by the engines at Prickwillow is about 25,000 acres; the drainage of a large area of higher land bordering on the Fens finding its way into this Fen drainage system. The water is lifted by both engines into the River Lark, about fourteen miles above Denver sluice, where the river discharges into the tidal stream from the same main Fen drain, which is 20ft. wide, with slopes 1½ to 1. The depth of water at starting the engines is generally about 6ft. 6in., decreasing to 4ft. 6in. after the pumping has been going on. Since the erection of the new engine and pump this drain has been found to be too small to keep up a full supply, the inclination on the surface being at the rate of six inches in a mile, which is greater than should be the case in a large main engine drain. The height the water has to be raised on an average is 10ft., rising as high as 17ft. in high floods in the river. Steam power was first applied to the drainage of this district in 1832, a 60-horse power low-pressure condensing engine being then erected by the Butterly Company to drive a scoop-wheel 33ft. 6in. in diameter; and this engine, with the aid of numerous wind engines previously in use, and retained as auxiliaries, preserved the district from injury fairly well. The continuous subsidence of the surface of the land and the increased height the water rose in the river, due to the rapidity with which floods now come down from the uplands, rendered this drainage power inadequate. It was found by experience that, owing to the constant variations in the levels of the water, both in the main drain and in the river, the scoop-wheel became so water-logged and unwieldy, and the loss by leakage so increased by the great head of 10ft. to 13ft., against which it frequently had to work, that, notwithstanding the great prejudice which all Fen men have in favour of the scoop wheel, Mr. Carmichael, the superintendent of the South Level, advised the Commissioners to adopt another form of machine which would adapt itself automatically to the variations of lift, and which, under the varying circumstances of the discharge, would absorb the whole power of the engine to the best advantage, and for this purpose he selected one of the Appold type, which, although they had been in use for some time in other parts of the Fens, were as yet untried in the South Level. The new engine and pump were intended to relieve the old engine of the greater part of its duty, more especially in times of excessive floods, and to drain out the water to a lower level than was practicable with the scoop wheel. The new machinery was erected by Messrs. Easton and Anderson, under Mr. Carmichael's direction. The engine is a 60 nominal horse power compound condensing beam engine, supplied with steam at 65 lb. pressure by two Lancashire boilers. The high-pressure cylinder is 15in., and the low-pressure 25in. diameter, with 4ft. 6in. stroke. The pump is of the vertical spindle pattern, with single inlet, with balance fan 5ft. 4in. diameter and 1ft. 2in. deep, placed at such a level that the lowest water in the drain will cover it. The inlet is 2ft. 8in. diameter, formed on the lower side only, special

provision being made for balancing, the weight of the column of water above the fan being balanced by the fixed inlet piece, which also serves to steady the lower end of the fan spindle. The meeting faces between the fan and the fixed case are both turned in the same direction, so that wear as it takes place can be taken up simply by lowering the fan spindle by means of an adjustment provided for the purpose. To take up the momentum of the water issuing at great speed from the fan, patent guide curves were fitted, which turned the water gradually into the vertical direction and at the same time assisted to bring it to rest. In this particular instance these guide curves were not found to be of much avail, as when the river was very low the delivery was lower than the top of the blades, and consequently there was a churning action going on with the water in the well, which caused vibration in the spindle. They were, therefore, removed. The pump is placed at the bottom of a brick well, in one side of which is the outlet passage 4ft. wide by 4ft. 6in. high, fitted with self-acting doors and communicating with a cast iron outlet pipe 4ft. 6in. diameter and about 68ft. long. The upper end of the fan spindle hangs in an onion bearing, and is driven by a pair of bevil wheels from a horizontal shaft which passes into the engine-house, on which is a pinion driven by annular gearing, bolted to the rim of the fly-wheel of the engine. The pump is calculated to lift 95 tons per minute at 8ft. lift, 88 tons at 9ft., 83 tons at 10ft., 78 tons at 11ft., 74 tons at 12ft., 71 tons at 13ft., 68 tons at 14ft., 65 tons at 15ft. The cost of the machinery, including engine, pump, and two boilers was £3853. The buildings, engine-house, boiler-house, pump well, chimney base, piling, and concrete, cost about £1064. At the trials which took place when the new engine was started it was

The height to which the water had to be raised was, however, reduced from about 9ft. to 4ft. In order, therefore, to thoroughly drain this district the Commissioners determined to provide better appliances for raising the water than those hitherto in use. Tenders for pumping machinery were advertised for, and that of Messrs. Appleby and Co. was accepted. The new machinery, the arrangement of which is shown in Fig. 12, was erected in 1877, and consisted of a scoop-wheel 24ft. in diameter by 4ft. wide, and, according to the maker's calculation, capable of delivering 3500 cubic feet (98½ tons) per minute to a height of 4ft., equal to 26.51-horse power of water lifted. The wheel makes five revolutions a minute, equal to a speed of 6.27ft. per second at the periphery. It is constructed principally of wrought iron. The scoops, eighteen in number, 10ft. long and 3½in. thick, are curved, and shrouded by wrought iron plates, and are connected to the wheel by curved arms, 2in. by 2in. by 3in. The sides are 3½in. thick at the periphery to 3in. at the centre. An adjustable curved shuttle is provided at the inlet to the wheel, by which the admission of the water is regulated. This shuttle is supported at the top by two arms, which project and clasp the axle of the wheel. Part of the pressure of the water against the shuttle is thus brought to bear on the axle, causing considerable friction. The cill over which the water is delivered is curved to the radius of the wheel. The wheel is keyed on to a wrought iron shaft 9in. in diameter, which runs in adjustable gun-metal bearings. On one side of the wheel is bolted a geared wheel made in segments, 20ft. in diameter, of 3in. pitch and 6in. face, and into this works the pinion on the engine crank shaft. The engines are of 40 nominal horse-power, of the horizontal high-pressure compound condensing type. The high-pressure cylinder is 10in. in diameter and 20in. stroke. The low-pressure cylinder is of 20in. diameter and 20in. stroke. The low-pressure cylinder and condenser are on one base, the air pump being fixed in the chamber of the condenser. The high-pressure cylinder is placed on a separate base parallel with the other cylinder. The fly-wheel is 9ft. in diameter. Steam for the engines is generated in two Cornish boilers, 20ft. long by 5ft. diameter, fitted with Galloway tubes, the safety valves being weighted to a pressure of 80 lb. of steam. The engines and boilers are contained in a brick building. The chimney is of brick, built square, 60ft. high. The contract price for building and machinery was £2680, of which £700 was for the buildings, chimney, and casing for wheel. This



SCOOP WHEEL AT NORDELPH.

found that the old engine indicated 103.33-horse power when delivering the water to a height of 9.78ft.; the new engine when indicating 106-horse power delivered 75.93 tons to a height of 10.84ft.; the coal consumption was at the rate of 2½ cwt. per hour, and as compared with that of the old engine in the proportion of 3 to 5. At a subsequent trial a weir 13ft. wide was placed across the outlet drain, the difference of level between the water in the inlet drain and the weir at starting was 8ft. 9in.; with the scoop-wheel the depth of water over the weir was 12in., with a lift of 9ft. 6in.; with the pump, the lift being 10ft., the depth of water over the weir was 13½in. The lift being increased about 3ft., the depth of water over the weir was 4in. less with the scoop-wheel than with the pump. At the trials that were made, the new engine indicating 106-horse power, 75.93 tons of water were lifted by the pump 10.84ft., equal to 56-horse power of water lifted, or an efficiency of 52.79 per cent. The old engine, indicating 103.33-horse power, the wheel lifted 71.45 tons to a height of 9.78ft., equal to 47.43-horse power of water lifted, or an efficiency of 46 per cent.; the coals consumed by the new engine were at the rate of 2½ cwt. an hour, or 5.50 lb. per horse-power of water lifted per hour. In ordinary working at the present time the consumption is at the rate of five tons in 30 hours for a lift of from 11ft. to 12ft. Taking the horse-power as before at 56, this gives 6.66 lb. per hour; or, if the work be taken at 74 tons lifted 11ft. 6in. high, a horse-power of 58.45, and coal consumption of 6.39 lb. The old engine and wheel consumes six tons of coal in 24 hours; if the horse-power be taken at 48.12 as before, this gives 11.64 lb. an hour. The cost of this pumping station, including both machines, on an average of the three years 1881-2-3, for coal, oil, attendance, &c., was £625, of which £483 was paid for coals, which represents about 644 tons. This is equal to a cost per acre for land drained of about 6d., or, taking coals only, 4.62d., and taking the average height the water has to be lifted at 9ft. 6in., this is equal to 0.80d. for all expenses, and 0.62d. for coals only per acre per foot of lift.

The *Upwell, Outwell, Denver, and Welney* south district is situated in the Middle Level in Norfolk, being part of the Great Bedford Level. This district was originally drained by scoop wheels driven by windmills. The quantity of land which is drained by the two wheels is about 9000 acres. The pumping station is at Nordelph, about three miles from Downham. It was anticipated that the construction of the new Middle Level drain in 1846 would do away with the necessity of pumping the water off the district, but experience showed that this was not the case.

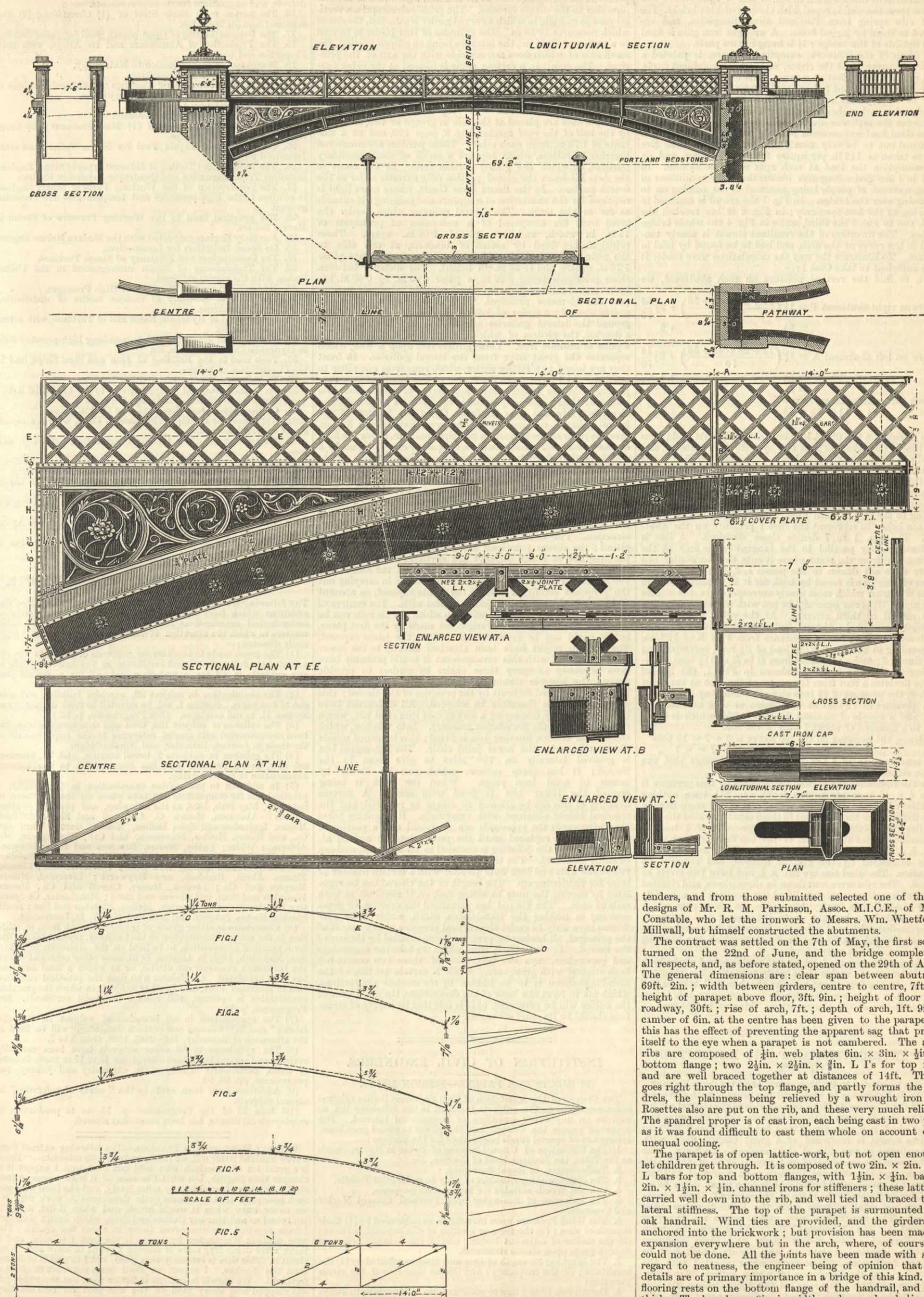
is equal to £74.68 per horse-power of water lifted for the machinery, and £26.40 for the buildings, together £101.08. This is the only wheel in the Fen-land that has curved blades. The head and dip of this wheel in ordinary floods are about 8ft. 6in. The relative proportions of each varying as the water lowers in the inlet or rises in the outlet drain. As an average the dip may be taken at 4ft. 6in. and the head at 4ft. With the wheel making five revolutions a minute, and allowing 20 per cent. for slip of water and leakage, and this deduction is borne out by the quantity of water flowing down the engine drain; the discharge is equal to 4305 cubic feet—120 tons—a minute. The quantity of coals consumed for this discharge, with 4ft. head, is about two tons in twelve hours, equal to 11.440 lb. per horse-power per hour of water lifted. By the side of the engine-house stands one of the old windmills which is still used to drive a scoop wheel 20ft. in diameter and 2ft. wide, and which when there is sufficient wind assists in raising the water from the district. When both steam and wind engines are at work the quantity as given above is about equal to the discharge of a continuous fall of ¼in. of rain in twenty-four hours over the area of 9000 acres, of which the district is comprised.

RAILWAYS AND POPULATION.—The following table shows the railway population and area of European countries at the end of 1885. The kilometre is .62 of a mile:—

Countries.	Total length in kiloms.	Area in square kiloms.	Population.	Kiloms. per 100 sq. kiloms.	100,000 inhabitants.
Great Britain and Ireland .. .	30,843	314,028	35,241,482	9.81	87.4
Belgium .. .	4,410	29,547	5,853,278	14.97	70.5
Luxembourg .. .	362	2,587	213,283	13.99	170.0
Netherlands .. .	2,468	33,000	4,336,012	7.47	56.9
Switzerland .. .	2,761	41,346	2,846,102	6.85	97.0
Germany .. .	36,779	540,599	46,852,450	6.80	79.1
France .. .	32,491	528,572	37,672,048	6.15	86.2
Denmark .. .	1,942	38,302	1,969,088	5.07	98.6
Italy .. .	10,354	286,588	29,699,785	3.61	34.9
Austria-Hungary .. .	22,341	622,310	37,882,712	3.59	58.9
Portugal .. .	1,527	88,872	4,306,554	1.72	35.4
Russia .. .	9,185	497,244	16,961,742	1.65	54.1
Sweden .. .	6,892	450,574	4,682,769	1.53	147.2
Roumania .. .	1,682	129,947	5,376,000	1.80	31.3
Greece .. .	524	64,689	1,979,561	0.81	26.5
Balkan Principalities .. .	2,122	374,961	10,889,391	0.56	19.6
Russia .. .	25,620	5,016,024	85,296,479	0.51	30.0
Norway .. .	1,562	325,422	1,981,000	0.49	80.9
Finland .. .	1,311	373,604	2,176,431	0.35	60.2
Europe .. .	195,176	6,885,423	337,354,068	1.97	57.8

RAVINE BRIDGE, LOWESTOFT.

MR. R. M. PARKINSON, A.M.I.C.E., ENGINEER.



RAVINE BRIDGE, LOWESTOFT.

The illustrations above show a bridge lately erected at Lowestoft over the Ravine, in the Belle Vue Park. This bridge has been presented to the town by Mr. Youngman, the first

mayor of Lowestoft, to commemorate the Jubilee year of her Majesty's reign, and was opened with some ceremony on the 29th of August last, that being the second anniversary of the grant of a charter of incorporation to the town.

Mr. Youngman advertised in our columns for designs and

tenders, and from those submitted selected one of the two designs of Mr. R. M. Parkinson, Assoc. M.I.C.E., of Melton Constable, who let the ironwork to Messrs. Wm. Whetford, of Millwall, but himself constructed the abutments.

The contract was settled on the 7th of May, the first sod was turned on the 22nd of June, and the bridge completed in all respects, and, as before stated, opened on the 29th of August. The general dimensions are: clear span between abutment, 69ft. 2in.; width between girders, centre to centre, 7ft. 6in.; height of parapet above floor, 3ft. 9in.; height of floor above roadway, 30ft.; rise of arch, 7ft.; depth of arch, 1ft. 9in. A camber of 6in. at the centre has been given to the parapet, and this has the effect of preventing the apparent sag that presents itself to the eye when a parapet is not cambered. The arched ribs are composed of $\frac{1}{2}$ in. web plates 6in. \times 3in. \times $\frac{1}{2}$ in. T I bottom flange; two $2\frac{1}{2}$ in. \times $2\frac{1}{2}$ in. \times $\frac{3}{8}$ in. L I's for top flange, and are well braced together at distances of 14ft. The web goes right through the top flange, and partly forms the spandrels, the plainness being relieved by a wrought iron bead. Rosettes also are put on the rib, and these very much relieve it. The spandrel proper is of cast iron, each being cast in two pieces, as it was found difficult to cast them whole on account of the unequal cooling.

The parapet is of open lattice-work, but not open enough to let children get through. It is composed of two 2in. \times 2in. \times $\frac{1}{4}$ in. L bars for top and bottom flanges, with 1 $\frac{1}{2}$ in. \times $\frac{1}{2}$ in. bars, an 2in. \times 1 $\frac{1}{2}$ in. \times $\frac{1}{4}$ in. channel irons for stiffeners; these latter are carried well down into the rib, and well tied and braced to give lateral stiffness. The top of the parapet is surmounted by an oak handrail. Wind ties are provided, and the girders well anchored into the brickwork; but provision has been made for expansion everywhere but in the arch, where, of course, this could not be done. All the joints have been made with special regard to neatness, the engineer being of opinion that small details are of primary importance in a bridge of this kind. The flooring rests on the bottom flange of the handrail, and is 3in. thick. The boards are 9in. in width, and are placed $\frac{1}{4}$ in. apart and coated with Stockholm tar.

The abutments and wing walls are constructed of cement concrete faced with brickwork varying from 9in. to 18in. thick. It was first intended to use lime concrete, but as time was an object, and unless care is taken in using it, this is liable to swell and displace the brickwork, it was thought better to use

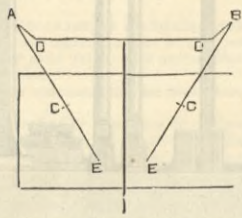
LETTERS TO THE EDITOR.

[We do not hold ourselves responsible for the opinions of our Correspondents.]

STRESSES IN A CAMP STOOL.

SIR,—The camp stool puzzle seems to get a wondrous complexity in small space, and I don't think the disputants will derive full benefit unless each breaks at least one camp stool for himself!

and a stable bucket with a can of water furnished breaking weights. First I secured a piece of board some 2ft. long to the window frame so as to project conveniently into the room.



W. A. S. B.

plified in the case of all flanged steam pipes, cylinder covers, &c., connected by bolts; the bolts are firstly strained by the nuts sufficiently to make the joints, and are subsequently further strained by the load due to the steam pressure.

If we compare the figure to an external fitted manhole-door and allow the area exposed to the steam pressure, multiplied by the pressure per square inch = 1 ton, then in such case the bolt will be strained as before, i.e., 5 tons due to tightening up, and 1 ton due to the steam pressure, total = 6 tons.

If we compare the figure to an internal fitted manhole-door the area exposed to steam pressure multiplied by the pressure per square inch = 1 ton, then in such case the bolt will be strained as before, i.e., 5 tons due to the tightening up; but the steam pressure will nullify 1 ton, reducing the strain on, say, the outer nut to 4 tons.

R. HARTLAND. Cork, August 23rd.

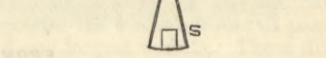
SIR,—The problem presented by "X." is our old friend the lock-nut in a new guise, and in view of a possibly protracted and more than likely barren discussion, it seems a pity that this should not at once be recognised and treated accordingly.

If we suppose that equal increments of load, by screwing or weighting, produce equal increments of deflection of the spring, then the problem is simple. If, however, the load on the spring is a curve, and not a straight line, we must first determine that curve, and this can only be done experimentally.

SIR,—Your correspondent "X." is evidently wrong if he assumes 6 tons to be the weight on top nut of his diagram. The bolt is subject to a strain of 5 tons due to the reaction of the spring.

J. H. K. August 30th.

SIR,—The puzzle offered by your correspondent "X." is readily solved by the methods of the kindergarten. A A is a lath, representing, for the purposes of this experiment, a rigid girder; B B are the halves of a wine cork nailed to the lath, say 3in. apart; C is a common red rubber band put round the nail heads; T is a loop of tape passing over the band and pinned to a scale pan S, made by folding a sheet of note-paper into a stirrup.



Now, put one ton in the stirrup, or any weight up to five, and no deflection marking additional strain will be observed in C. The weight merely relieves the pin P—which corresponds to the lower nut in "X.'s" diagram—of so much of the upward pull of the spring.

W. A. S. B. August 30th.

ACCIDENTS ON TRAMWAYS.

SIR,—In reference to your notice on the above in your last edition, stating "that the accidents are causing an increasing demand to be made by the public for life-saving appliances to be attached to the engines," I beg to state that I studied this question during the time I was in charge of several tram lines at home and abroad.

As to the practical application of lifeguards, may I be permitted to state that practical experience has proved that they are more dangerous than no guards, and assist rather more to increase than to prevent injury.

H. CONRADL. 13, Soho-square, London. August 28th.

IBBOTSON'S LOCK-NUTS AND FISH-BOLTS.

SIR,—Being the sole makers of the Ibbotson's patent steel expansion lock-nuts and special steel fish bolts used on the Great North of Scotland Railway, our attention has this day been drawn to an article under the head of "Railway Matters" at the foot of page 169 of THE ENGINEER, No. 1652, of the 26th inst., containing a quotation from the report of Colonel F. H. Rich on the accident which occurred on the 16th May last between Buckpool and Port Gordon Stations on the above-named line, wherein he questions whether the fish-bolts and nuts used on that railway can be con-

sidered safe, because he concluded that they were, to some extent at least, the cause of the buckling or bending of some of the rails discovered there, owing to the excessive tightness with which they were found to grip the rails at their joints.

We should be greatly obliged if you will permit us to state in your paper that as our lock-nuts do become securely and firmly locked on any part on the bolt up to which they are screwed, there is no necessity whatever that they should be screwed up so tightly as to prevent the expansion of the rails.

The fact that such an extraordinary gripping force can be applied by their use is undoubted, but if so applied, care should be taken when any marked change of temperature sets in to slacken the nuts back a little to permit the rails to expand or contract as the case may be.

No slackening back and re-tightening up of our nuts renders them in any way loose upon their bolts, or diminishes to any appreciable extent their tight gripping hold thereon.

IBBOTSON BROTHERS AND COMPANY, (ALFRED B. IBBOTSON, The Patentee and Managing Director.) Globe Steel Works, Sheffield, August 29th.

THE STRESSES IN THE IOWA BRIDGE.

SIR,—In reply to Mr. Cunningham's letter, I would remark that it depends altogether on the character of the "internal modifications" whether the main truss, which without the "twist" can be adapted to either form, becomes a Warren or a Whipple girder. An American would generally adapt it to the latter type.

I must also maintain that an "arch" is named in virtue of its form and not of its thrust. A thrust is not the exclusive property of an arch; it also belongs to such widely different types as braced iron piers and certain roof trusses.

R. H. GRAHAM. August 31st.

MARINE ENGINE BEARINGS.

SIR,—In your article on "Marine Engines from a Shipowner's Point of View" you speak of the internal friction being 15 per cent. or more. It has often occurred to me that marine engine makers might take a lesson from the makers of a very different sort of machine, viz., the tricycle.

[Roller bearings might be used in a screw tunnel, but we doubt that they could be used in an engine-room, as any slackness of bearing would cause them to be hammered to pieces.—ED. E.]

A CURIOUS EXPLOSION.

SIR,—An explosion recently occurred at a paper mill, the particulars of which are as follows:—During the admission of caustic liquor into the ovens in the process of recovering the caustic soda used for washing esparto, an explosion occurred resulting in the complete demolition of an oven, and serious injury to the man attending same.

As a matter of fact the oven in question was in a perfectly safe condition, constructed of the best fire bricks, the piers being 18in. thick, although, of course, this was reduced in some places by burning.

The theory of the defendant was, that the man allowed the oven to become overheated, and the liquor to enter the oven too rapidly, thus causing a steam explosion; and that the accident happened entirely by reason of the man's neglect and carelessness.

Being non-suited, the plaintiff appealed, and on the second trial recovered heavy damages. On this occasion the theory of "the cold air rushing on the hot" was abandoned, and no explanation whatever was offered to account for the explosion, other than the collapse of the oven.

Now there is no doubt a violent explosion occurred, the debris being carried some distance, and I can find no other cause for it than that mentioned above, viz., a steam explosion caused by the liquor flowing into an overheated oven.

As the intelligent British jury gave a verdict for the plaintiff, they of course believe in the curious coincidence that the crown of the oven fell at the precise moment that the liquor was allowed to flow.

CHAS. FREDK. FULLER, C.E. Bow-lane, E.C., August 31st.

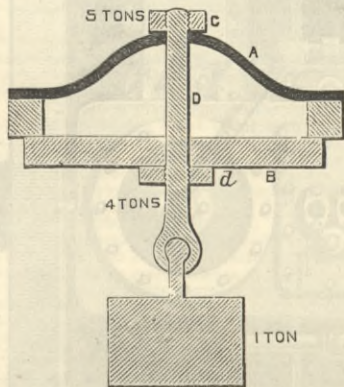
FEATHERING PADDLE WHEELS.

SIR,—Professor Greenhill in his interesting letter in your last impression seems to have overlooked the circumstance that the proper angle of the float varies with the speed and slip. A vessel steaming at a very high speed scarcely needs to feather her floats at all, because the floats move rapidly away from the water.

M. E.

A PROBLEM IN STRAINS.

SIR,—With reference to the letter of your correspondent "X." last week, the second party he mentions are undoubtedly right, for the bolt between the nuts has an extension λ varying directly as the pressure, according to Hooke's law.



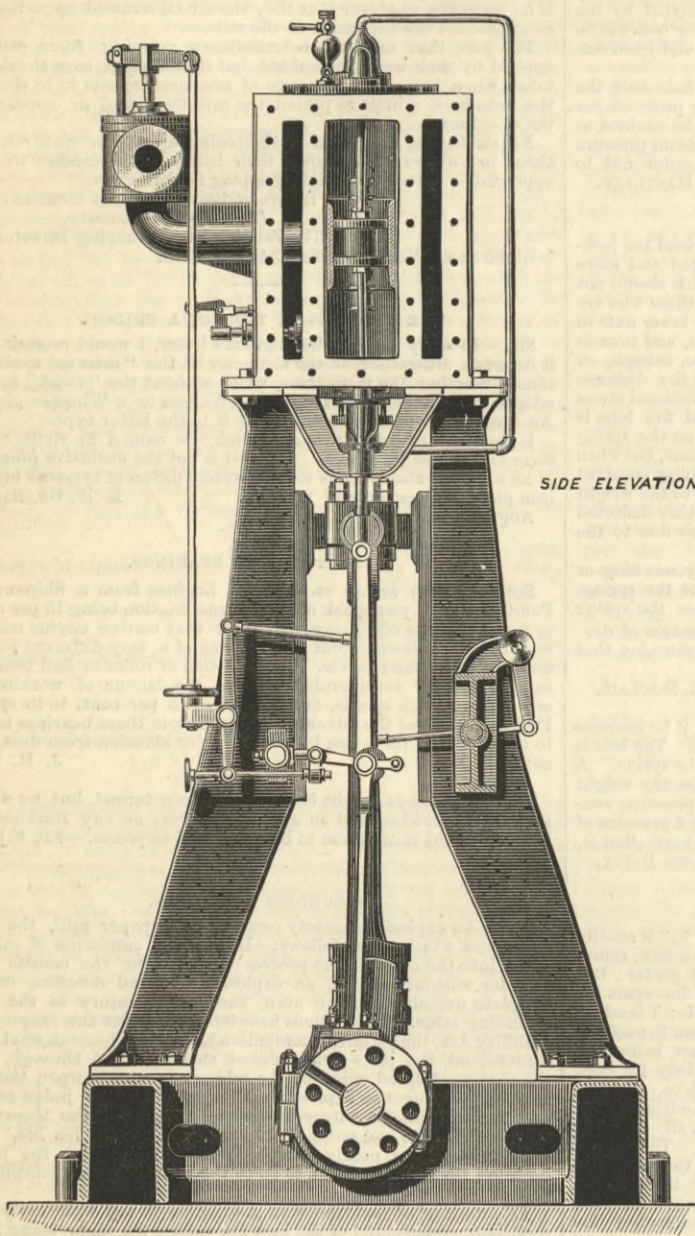
the pressure of the lower nut. In fact, as long as the extra weight does not exceed five tons, so long does the bolt remain the same length, and so long does the pressure on the upper nut = 5 tons and the pressure on the lower nut = 5 tons, less the extra weight.

T. E. N. August 23rd.

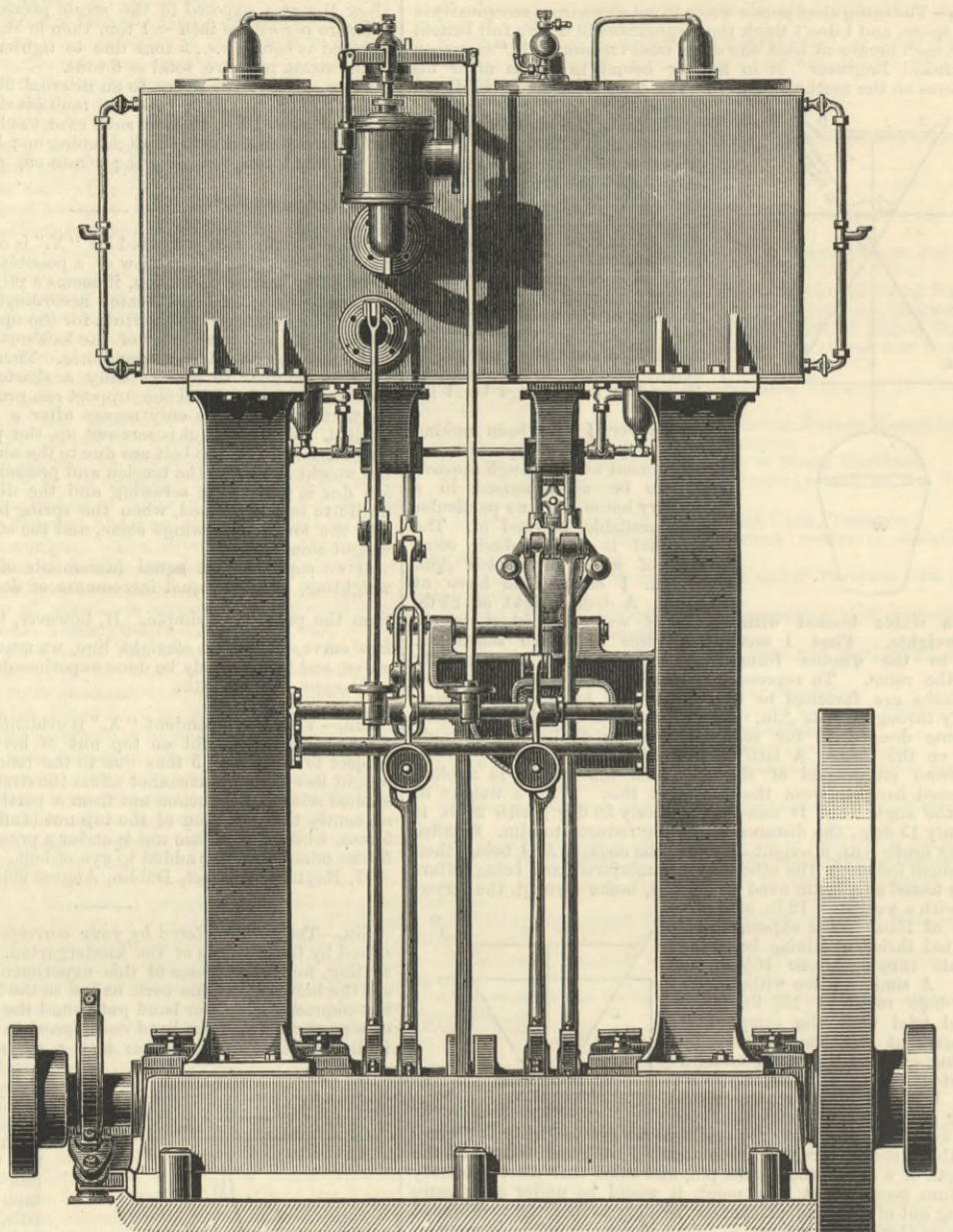
SIR,—Referring to "X.'s" letter in last week's issue, Newton's third law states that to every action there is always an equal and contrary reaction, therefore the strain due to the 5 tons tends to break the bolt across somewhere between the nips of the nuts.

COMPOUND VERTICAL ENGINE, INDIAN STATE RAILWAYS.

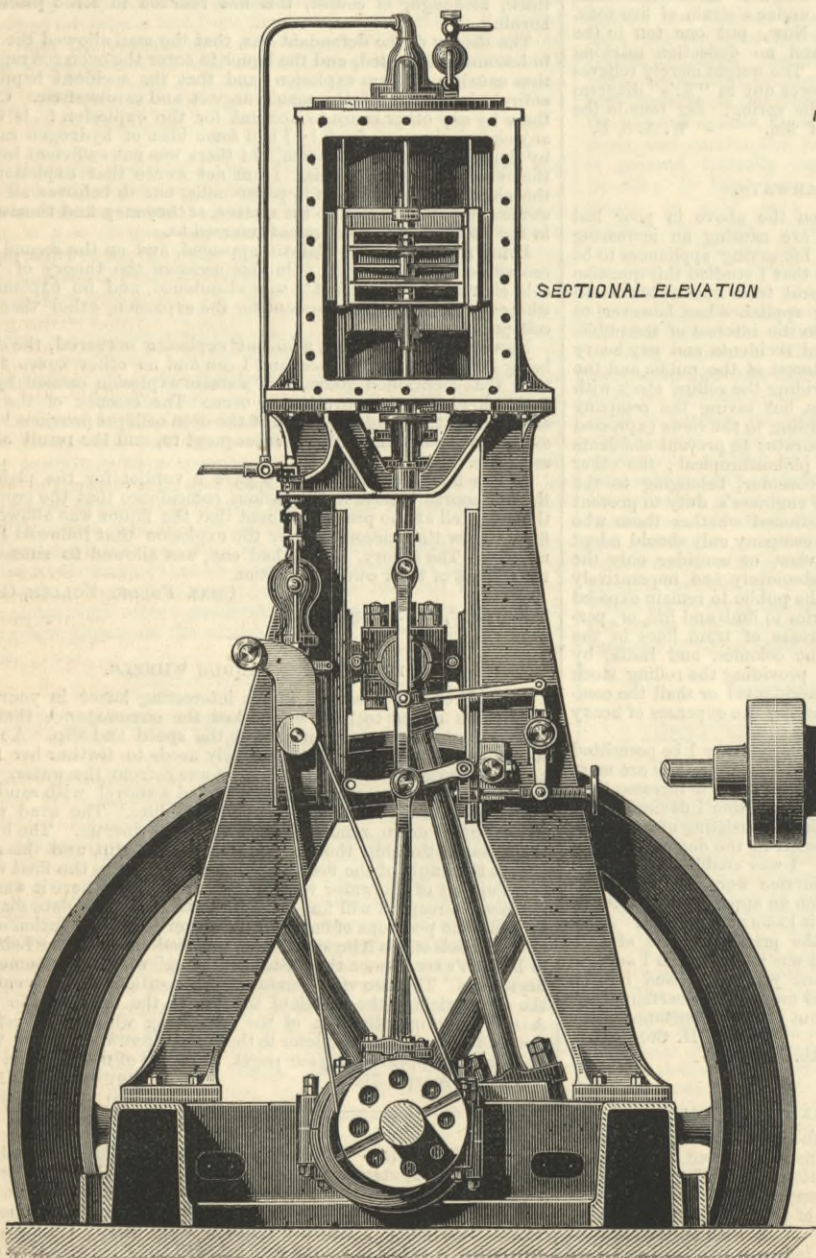
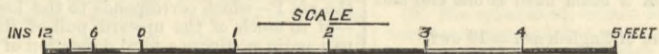
(For description see page 198.)



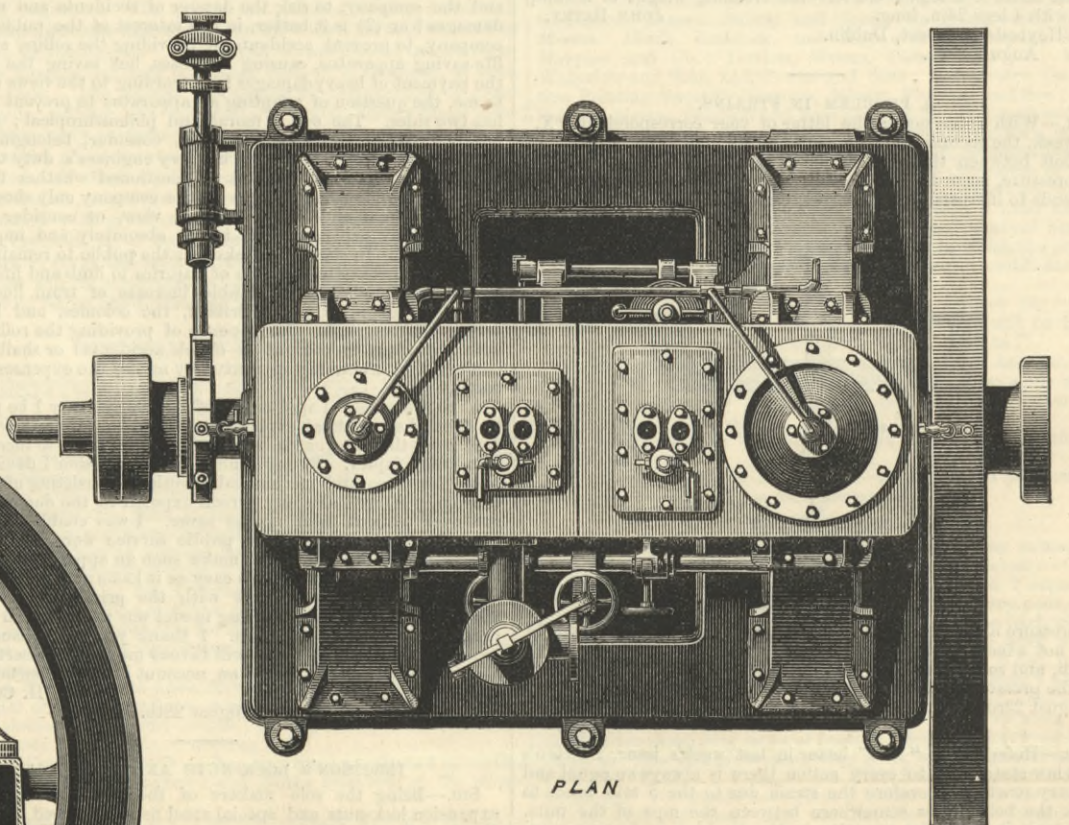
SIDE ELEVATION



FRONT ELEVATION



SECTIONAL ELEVATION



PLAN

lated according to the number of passengers for which she is fitted, or according to her load displacement. Thus, in the case of a vessel entirely employed in cargo carrying, only the degree of sub-division presently existing might be imposed, or it might simply be left to the care of the insurance and registration societies on the grounds that the boat accommodation would be ample for the use of the crew in an emergency. In the case of a vessel carrying passengers chiefly, and especially when the number is of necessity greater than there is boat accommodation for, sub-division should be regulated by a comparison of the actual with the possible floating displacement. In other words, the sizes of the several compartments into which the vessel would be divided should be regulated—as is at present the case with vessels on the Admiralty List—by the amount of surplus buoyancy of which she is possessed. In no case should there be any two compartments of greater capacity than, if filled, the vessel would sink. Such regulations, however, the Advisory Board, constituted as proposed, would find easy of adjustment. Whatever measure of approval the other recommendations of the two reports may meet with from Government, or the public at large, it is to be hoped that this matter of an Advisory Council will commend itself entirely to all concerned. Its institution would definitely further the cause of live-saving at sea to an extent for which, as experience has already shown, we may look long and vainly from Committees of enquiry merely.

GERMAN COMPETITION WITH BRITISH SHIPPING.

We recently devoted an article to the results now ascertained to have followed from the system pursued by the German Government of granting bounties to those of its subjects who became proprietors of shipping. It was shown in that article that those bounties were insufficient in amount to ensure profitable results to German owners in the fierce competition to which restricted trade and superabundant tonnage had given rise during the last few years. But although such has undoubtedly been the issue to the system, it is impossible to be blind to the fact that the bounty system has worked severely against the British shipowner in this competition. It could hardly be otherwise—at least in some trading directions. German shipowners start well handicapped by the bounties referred to; they are free from restrictions imposed by Government regulations on our own shipowners, and their crews are almost invariably composed of men among whom as yet the evil side of trade unionism has not been developed, while they will accept lower wages than are demanded by the sailors and others of the crews of our own mercantile marine.

It will be of interest to note any facts which tend to show how far in this war of competition the interests of British shipowners have become affected. A single instance—which is typical, however, of some others of similar character—may be quoted in illustration. We have it on official authority that although in 1880 the German tonnage finding employment at the port of Nagasaki, in Japan, was less than one-twelfth of the British tonnage working that port, it had risen in 1886 to one-third of the figures denoting the latter. Moreover, we learn from the same official source that during the interval between the two years named, the German tonnage employed had increased *tenfold*, while that of British nationality had but little more than doubled. Now, looking at this single instance, and regarding it, as we believe we must do, as being illustrative as to what has taken place in the same interval of time at many other places where the British and German mercantile marine are competing, it must be admitted that it opens out ground for much fear for the future. We see that during the years in which British tonnage has been to a large extent laid up as unable to find profitable employment, German vessels have been active in superseding us in the trade that might, had conditions been more favourable to our own ships, have been secured for them. We have before asserted how difficult it is when the course of trade flows towards the ships sailing under one flag for those registered under another to divert it. Prominence was given to that contention in the article above referred to when pointing out how hard must be the conditions under which Germans would have to secure trade already carried by ourselves. We cannot therefore disregard the evidence given by the figures above quoted that, in some degree at least, the Germans have been successful in overcoming that difficulty. The argument we employed against them is, in this instance, turned against ourselves.

Some of the reasons, and those the most patent, which have tended towards obtaining that success we have referred to above, and their potentiality and their certain effect cannot be denied. Nor do we see the least reason to hope that the restrictions which our own advanced civilisation imposes upon us have the least prospect of being soon balanced by other nations following our humanitarian lead with respect to them. They must, therefore, remain for an altogether indefinite period a heavy incubus on the British shipowner in his competition with the foreigner. But the question presents itself to our mind as to how far such disabilities would stultify us in such a competition did they stand alone. We believe in British pluck, energy, and skill being quite equal to counterbalancing them, and must seek, therefore, for some other factor weighing against us in the race. We fear we have not to seek far for it. The same characteristics, which are largely conducive to the ousting of our own countrymen in London, are telling in the department of which we are writing. The foreigner can and will do more, and for less pay, than our own people, and the British shipowner must either ship crews of foreigners or be as worsted in his contest as is the London clerk. We do not write of this matter without experience to warrant our doing so. We have lain alongside of ships in Eastern ports, and have seen that at the striking of the four bells of the evening the British sailor has laid down every load and ceased work, however urgent may have been the demand for the dispatch of his vessel. On

the German or Norwegian ships alongside, their crews have pursued their task until it was completed.

How severely this indisposition to meet exigency tells against the British shipowner, may be gauged by a further statement of the official report to which we have made reference. It says:—"Charterers decidedly prefer German to British vessels by reason of the dispatch given by German shipmasters, in a great measure due to the ready and indefatigable assistance of the officers and crew, which compare very favourably with the attitude frequently assumed in other cases. In the case of one large shipping firm, owing to these reasons, it can always afford to give better terms to the Germans." We fear we must not rely too much, while such distinctions are possible between our own and foreign practice, on the failure of the German bounty system to stay the evil effects to ourselves of foreign competition. As a nation, we are possessed of many advantages which are not given to the foreigner. They enable us to make head to some extent against the cheaper labour by which his vessels are worked; but there are moral disabilities, it is certain, which must be removed if we are to cease in the future to see British shipping supplanted by our German friends to the extent that it has been of late years at the Port of Nagasaki and elsewhere.

AEROSTATION AND AERONAUTICS.

THREE years ago we had occasion to refer to a balloon voyage accomplished in France by Captain Renard, at that time director of the balloon works at Meudon, and Captain Krebs, his assistant. The voyage was remarkable as being apparently a successful attempt to navigate a balloon, and the rate of travelling was not altogether slow. The account given was that the balloon went seven miles out, travelling against the wind, and then came back again, so as to descend at the point from which the aeronauts originally started. This was, therefore, an instance of actual aerial navigation. M. Hervé Mangon presented a report on the subject to the French Academy of Sciences, and declared that August 9th, 1884, the day on which the feat was accomplished, would be "for ever memorable in the annals of discovery." The world has not been much the better for the discovery so far. For land journeys we have still to rely on the railway service, and if we seek to cross the ocean there is nothing superior to a big steamship. A sensational ascent has been recently effected by MM. Jovis and Mallet in the balloon *Horla*, the object being to reach the greatest practical altitude, which in this instance proved to be 7100 metres, or rather less than 4½ miles, whereas Mr. James Glaisher, accompanied by Mr. Coxwell, ascending at Wolverhampton, in 1863, attained an altitude of about 7 miles, though at the imminent peril of life. But M. Jovis has something yet in store. According to the account of an interview with this gentleman by a representative of a daily contemporary, M. Jovis is going to undertake a balloon voyage from New York to the coasts of Europe. The wisdom of attempting to come rather than to go is evident. The chance of a favourable wind from the west is far greater than one from the east. M. Jovis will wait at New York until a convenient storm presents itself, and will then make his start on the wings of the tempest. "You expect to leave New York in October, I believe?" said his interrogator. "It is impossible to say," was the reply. "We may have to wait till December, or even January, for an atmospheric disturbance which may be expected to cross the Atlantic and pass along our coasts." The utility of all this seems doubtful. To wait for an indefinite period, and yet to be always ready to start, will fail to suit the convenience of an ordinary traveller, however well it may adapt itself to the designs of M. Jovis. Simply to go the way the wind blows implies nothing very scientific. On this plan, at some date inside the next twelve months, M. Jovis may undertake to go anywhere within a range of three thousand miles. What possible good there is in this project for an Atlantic voyage we cannot see. The affair is "sensational," like the recent ascent, and we are at a loss to make anything else of it, supposing the scheme to have any real existence. The balloon is to be called "*La France*," and is expected to be complete about the end of the present month, when it will be packed up and taken from Paris to New York. It is to have a diameter of 27 yards, but 8477 cubic yards is said to be the extent of the capacity. This would be about 13,500 cubic feet beyond the size of the great balloon in which M. Nadar made two ascents in the autumn of 1863, when he expected to steer by means of a screw. The balloon in which M. Jovis proposes to cross the Atlantic will therefore be the largest yet made. When Professor Wise was intent on an aerial voyage from New York to Liverpool, in 1873, he proposed to employ a balloon yet larger than that which M. Jovis contemplates, the horizontal diameter being 100ft., and the vertical axis 110ft. There was also to be a supplementary balloon, with a diameter of 36ft. Despite the great size of the main balloon, it was reported to be inadequate for the task to which it was to be devoted. If this conclusion were correct, M. Jovis appears to be seriously under-estimating the conditions of success. However, he is said to be busily engaged in superintending aeronautic affairs at the headquarters of the French Balloon Society in the Boulevard Clichy. His assistant, M. Mallet, is to accompany him in his Atlantic voyage, and it is reckoned that the transit from New York to Europe will only occupy from forty-eight to sixty hours. The balloon is believed to be capable of keeping aloft for a period of four days.

But Captain Renard, now Chief of the Military Balloon Service at the camp of Chalons, is once more on the scene, and promises to excel his former achievement. Instead of making headway, as in 1884, against a current having a velocity of five metres per second, he undertakes to resist a current of double that strength. This means that his balloon is to be propelled, in virtue of some self-contained power, at a rate exceeding ten metres per second, or 22 miles per hour. On the former occasion the balloon

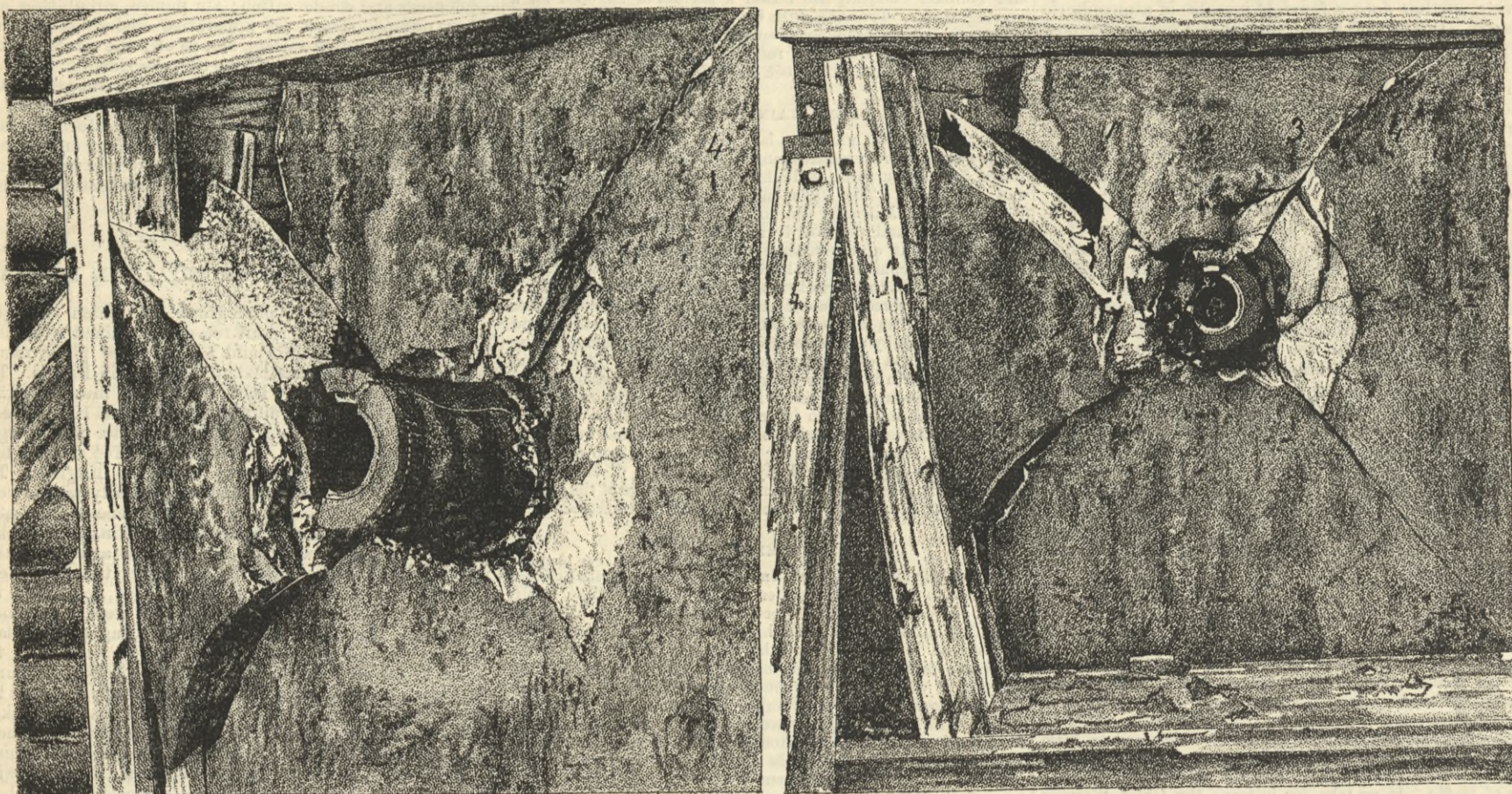
was said to have travelled 14 miles in about 40 minutes half this distance being accomplished against an aerial current of about 12 miles per hour. Supposing these data to be correct, we reckoned that the inherent speed of the balloon must have been 26 miles per hour. Facing a current of 12 miles per hour, a balloon so propelled would have a geographical velocity of $26 - 12 = 14$ miles per hour. It would therefore expend half an hour in going out seven miles; but in returning it would have a geographical velocity of $26 + 12 = 38$ miles per hour, and would therefore accomplish the return journey of 7 miles in 11 minutes. The entire trip would accordingly occupy 41 minutes, the time stated being "about 40 minutes." To drive a balloon along at the rate of 26 miles an hour is no small achievement. In commenting on this affair in 1884 we recorded our opinion that the narrative was "extraordinary," and we expressed a desire for some explanation. Now at last we find it stated that Captain Renard is going to travel faster than ever. There is a slight reduction in the velocity of the current which is said to have been encountered three years ago, but the discrepancy is simply 11 miles per hour instead of 12, and the coming feat is to consist in resisting a current equal to 22 miles per hour. So far as mere "resistance" goes, Captain Renard could have coped with such a current as this in 1884. The geographical speed under such conditions would have been $26 - 22 = 4$ miles per hour. This would be slow travelling, but still it would be something. But even if Captain Renard has really succeeded in doubling his propelling power, it does not follow that he has practically solved the whole problem. To give a balloon an inherent velocity of fifty-two miles an hour is to do battle with the storm, and to encounter an atmospheric pressure equal to more than 12 lb. on the square foot. If the line of propulsion is below the central line of atmospheric resistance, a balloon propelled with a force equal to this would speedily turn a backward somersault and the car would find its way to earth. If, on the other hand, the line of propulsion coincided with the line of resistance, the balloon would simply be torn to shreds. The fact must be that there is an error as to the speed of the current in 1884, and also the distance travelled over. Fourteen miles in 40 minutes means twenty-one miles per hour, without taking any current into account. This of itself is equivalent to a brisk wind, exercising a pressure of more than 2 lb. on the square foot. The present project is that of facing a current travelling at the rate of twenty-two miles an hour, and if the former affair is to be considered as correctly reported, the forthcoming speed—if it is to be doubled—must be above fifty miles an hour. Possibly something less than doubling the inherent velocity of the balloon is contemplated, although a current of two-fold force is to be overcome. But at least thirty miles an hour must be reckoned upon, and forty would seem more in accordance with the promise given. The latter speed would occasion a pressure of nearly 8 lb. on the square foot of a flat surface struck perpendicularly.

But we may carry this matter a little further. The apparatus employed in 1884 is said to have included the use of certain electric accumulators, capable of supplying the power of ten horses for four hours. According to the account given, the balloon must have been propelled at a velocity exceeding twenty miles an hour. We will simply calculate on this basis, involving a pressure of 2 lb. on the square foot, supposing the surface to be flat and the force perpendicular. From this we will make a reduction, as the balloon presented an oblique surface to the impact of the atmosphere. To give the scheme every chance, we will put the pressure as low as 1 lb. per square foot of the sectional area of the balloon. But if the speed is to be doubled the resistance will be quadrupled, making the pressure 4 lb. per square foot. Discarding the force requisite to raise the balloon, we will simply consider the atmospheric resistance in a horizontal line. The propelling force derived from an engine of 10-horse power is equal to 330,000 lb. per foot per minute, or 1 lb. at the rate of 330,000ft. in a minute. Twenty miles per hour is equal to 1760ft. per minute, which, with 10-horse power, allows a total resistance of 187 lb. At the rate of 1 lb. per square foot this gives an area of 187 square feet, corresponding to the sectional area of a sphere having a diameter of about 15½ft. Captain Renard's balloon is described as elliptical in form. If we take it as equivalent to a cylinder having a length equal to 60ft. on a diameter of 15½ft., the length is as great as symmetry and safety would permit. This would give a cubical content of 11,220ft. The enclosed gas is not likely to have a greater buoyancy than one ounce per cubic foot. Hence the gas would lift 700 lb., from which the weight of the envelope must be deducted. Of course, a much larger balloon must be intended, with a corresponding increase of the sectional area and the atmospheric resistance. The speed, also, is to be doubled, raising the pressure to 4 lb. per square foot. Calculate as we will, we are at a loss to understand how anything like the expected speed can be obtained. Neither can we understand the results said to have been achieved three years ago. That something may be done in the way of propelling and steering a balloon we will admit. The steering is distinctly dependent on the propelling power, and this has to contend with the resistance of the atmosphere to the passage of the balloon, presuming that the gas gives sufficient buoyancy in the first instance. The balloon must be allowed some amount of dead weight, in order for it to be manageable; but this need not be much, and we have favoured the adventure by not taking this load into account.

The prospect of navigating a balloon with a useful velocity through the air seems very remote. But Captain Renard is sanguine, and the fact that he went out and came back again on the same line of route is certainly enough to make a man think that he can do something. His balloon must have possessed some inherent velocity, and, therefore, some steering power, in order for this to be accomplished. But the state of the atmosphere, and the distance traversed in the forty minutes, are elements which require to be carefully and

EFFECT OF A ST. CHAMOND PROJECTILE ON A STEEL-FACED PLATE.

(For description see page 197.)



carried past the excavation in temporary channels, there being a difference of 18ft. in the levels of the highest and lowest springs within the dell. This enabled two wells to be sunk on the high ground above the reservoir, in which the water stands 15ft. higher than in the reservoir itself. The wells are discharged by means of 4in. cast iron syphons, arranged so as to be self-charging. These are connected to the suction main leading to the pumping-engines, and by means of by-pass-valves can either or both deliver to pumps or reservoir. The water of the various springs below the level or the wells is conducted into the reservoir below the water-line, and is stored to give power for working the pumping-machinery.

During the time the pumps are working the water of one well is sufficient to supply them; the syphon of the second well therefore discharges into the power reservoir, and when the pumps are shut off both wells are so available. The necessary working pressure is obtained by placing the pumping machinery at a distance of 900ft. from the power reservoir, there being a fall of 65ft. in that distance. The driving water is conveyed from the power reservoir in a 6in. cast iron pipe, which passes through the embankment above a 9in. cast iron wash-out pipe with stand-pipe overflow within the reservoir, and are surrounded with cement concrete. The valves from the power and wash-out pipes are worked from a bridge in the usual manner. The suction pipe to the pumps is laid beneath the footpath on either side of the power reservoir, and after leaving the embankment is laid in the same trench as the power pipe, and has an available head of 70ft. above the pumps. The power reservoir contains 400,000 gallons, and the wells are capable of yielding about 120,000 gallons per day. The pumping machinery has been specially designed for these works, and was manufactured at New York, U.S.A., by the Worthington Pumping Engine Company, of New York and Queen Victoria-street, London, and is the first water motor of that company's manufacture erected in England, although their steam pumps are well known here, and several waterworks in the United States are supplied by their water motors. In these works two motors are used, one for high level and the other for low level duty, space being left in the engine-house for duplicate sets. The duty required is 45,000 gallons per day to be delivered 220ft. and 320ft. above the pumping station. The high-level motor has two motor pistons, each 5in. diameter by 9in. stroke, with two pumps each 2 1/2 in. diameter and 9in. stroke, with an average piston speed of 20ft. per minute. The low-level motor has two motor pistons, each 9in. diameter by 9in. stroke, with two pumps each 4 1/2 in. diameter by 9in. stroke, and having an average speed of 22ft. per minute. The motors are arranged side by side, and are in appearance similar to a horizontal steam pump. The power pipe enters at the centre of the engine-room, and delivers right and left to each motor. The suction pipe is brought in above the power pipe, and similarly delivers right and left to the pumps. The pumps deliver into a 4in. cast iron main for the low level and 3in. main for the high level, a by-pass being arranged so that either or both can deliver into either main. Owing to the special arrangements of the valve motion, there is an entire absence of shock, noise, or vibration.

The water used for driving is about four times the quantity lifted, thus comparing favourably with the hydraulic ram, while the slight attention required is a valuable feature. Pressure gauges are arranged upon the pumping mains, so that the attendant can at once tell what portion of the district is being supplied, and the motors automatically govern themselves according to the duty required of them. They have been run as a test for 120 hours without attention or inspection, doing continuous and regular duty during the period. The low level main delivers the water into a storage reservoir containing 27,000 gallons. The reservoir is excavated in the ground at the top of the hill above the pumping station. It is 27ft. 6in. diameter by 8ft. deep, constructed of 9in. brickwork in cement with 9in. concrete backing, and is covered by three 4 1/2 in. brick arches springing from wrought iron girders supported by two cast iron columns. The arches are covered with concrete and finished with 18in. of earth. The service pipe is arranged so that the pumps can deliver into the mains independent of the reservoir. As the high level reservoir is not yet constructed, the district above the 500ft. contour is supplied by continuous

pumping against a valve fixed within the low-level reservoir, into which any surplus water is delivered. The length of water mains, 5in., 4in. and 3in. diameter, at present laid is about 6 1/2 miles of cast iron 1/2 in., 3/4 in., and 5/8 in. thickness, and coated with Dr. Angus Smith's composition. Eighty per cent. of the joints are turned and bored, the unbored portion of the socket being filled in with Portland cement. A large area can yet be supplied by gravitation only. Where lead joints are made no yarn has been used, the joint being first caulked with drawn lead wire and afterwards run and caulked. The mains have been tested to a pressure of 150 lb. per square inch, and the pumping mains to 220 lb. per square inch in the open trench as the work proceeded. The working pressure upon the mains varies according to locality from 140 lb. to 50 lb. per square inch. The works have had the advantage of Mr. Kinsey being a resident of Oxted, and his consequent personal supervision, in which he has been assisted by Messrs. John T. Sample and G. Van Notten Pole, Studts. M. Inst. C.E., as clerks of works. Each line of main is provided with a district meter, a royalty being payable to Mr. Gower upon the quantity of water consumed. Messrs. G. F. Baker and Sons, Southwark-bridge-road, London, are contractors for the entire works. Messrs. Stone and Co., Deptford, supplied the valves and fittings, and Messrs. J. Tylor and Sons, Newgate-street, London, the meters. The cost of the works has been about £5000. As an illustration of an economical and effective arrangement for the supply of small districts from their own watershed, these works are interesting, and show how readily the springs which in many localities are wasted may be made a source of power and a benefit to the inhabitants.

COMPOUND VERTICAL ENGINES, INDIAN STATE RAILWAYS.

THE engravings on page 194 illustrate a vertical compound engine for which tenders were recently invited for the Indian State Railways. The engines are to have cylinders 10in. and 16in. diameter, and 24in. stroke, the revolutions to be 90, the steam pressure 90, and is to be tested and indicated up to 50 indicated horse-power. We shall in future impressions publish detail drawings of this engine fully dimensioned, which will, we think, be found useful and instructive by our student readers.

DESCRIPTION OF THE NEW TAY VIADUCT.¹

By MR. FLETCHER F. S. KELSEY, M. Inst. C.E.

Site.—The new viaduct across the Tay near Dundee, which has once more established direct railway communication between the counties of Fife and Forfar after an interval of nearly eight years, is situated throughout the extent of the straight portion, which forms four-fifths of its total length, at a distance of 60ft. centre to centre from the old structure. At the north end of the straight a curve of 21 chains radius gradually reduces the distance between them until they join in a common centre line at the point where they cross the esplanade at Dundee. Unlike the old viaduct, the new one carries a double line of railway, and consequently gains enormously in stability from the greatly increased width of the piers.

Dimensions.—The chief dimensions of the new work are as follows:—

Table with 2 columns: Description and Dimensions. Rows include: South end of Wormit arching to high girders (3585ft.), High girders (3156ft.), North end of high girders to north end of viaduct (3786ft.), Total length = 23ft. short of 2 miles = 10,527ft., Width between parapets (25 ft. 6 in.), Maximum width of piers at base (55 ft.), Minimum (36 ft.), Maximum headway above high water (77 ft.), Maximum height of rails above high water (83 ft.), Minimum (25 ft.), Maximum height of piers from foundations to top (141 ft. 6 in.).

There are in all eighty-six spans, five of which consist of brick arches and the remainder of girder work. Of the brick arches, four of 50ft. span are situated at the southern end of the viaduct, and one of 25 1/2 ft. at the northern end.

Piers.—Seventy-three of these have cylinder bases and may be

divided into two groups thus:—Group 1, comprising forty-nine constructed with wrought iron cylinder bases; Group 2, comprising twenty-four constructed with cast iron cylinder bases. The former are in the straight and the latter in the curved portion of the viaduct.

Cylinders.—The portion of the pier below low water consists of two of these cylinders, which, in the case of the piers for the thirteen large spans in the centre of the river, are placed at a distance from each other of 32ft., and in the rest of the piers 26ft., centre to centre. Except in the case of those for piers Nos. 5-14, the cylinders are all splayed at the base, and have a base diameter varying from 10ft. up to 23ft. The 10ft. cylinders which form the bases of twenty-four of the piers in the curve are of cast iron, all above this size being of wrought iron, and made of such a length that when sunk to the required depths the tops might project slightly above low-water level. They are all lined with brickwork filled in with concrete.

Blue-brick shafts and connecting-piece.—From low-water up to high-water level the piers in Group 1 consist of two circular blue-brick shafts of 12in. less diameter than the cylinders. They are filled in with concrete and joined together at high-water level by means of a strong connecting-piece, which also consists of blue brickwork filled in with concrete, the portion between the shafts resting on cast iron girders. In the cast iron cylinder piers—Group 2—the cylinders are continued up to the connecting piece, and cast iron segments of cylinders and plates take the place of the blue brickwork in the connecting-piece itself.

Base of pier superstructure.—On the top of the brickwork, and forming part of the connection, a wrought iron framework made chiefly of channel irons is placed, and securely attached to the shafts below by means of sixteen holding-down bolts of 2 1/2 in. diameter and 20ft. length, which are embedded in the masonry. This framework forms the base for the upper portion or superstructure of pier, which is rivetted to it.

Superstructure of piers.—In the case of piers Nos. 5-64, the superstructure consists of two wrought iron octagonal shafts, as shown in the engraving joined together near the top in the form of an arch; and is composed of plates connected at the angles by means of two splayed channel irons on the outside, and an obtuse angle iron on the inside. Outside and inside T-irons cover the other vertical joints, and serve to stiffen the structure, which is further strengthened by means of bracings and horizontal diaphragms placed at intervals inside the shafts. Short cross girders near the top support the cast iron bed-plates for the main girders. The height of these pier superstructures varies from 20ft. to 68ft. In piers Nos. 65-77 the superstructure and connecting piece are combined, on account of the reduced height of the piers, and assume the form of a tapered box, stiffened with channels and tees in the same way as the rest of the piers.

Cylinder sinking.—In sinking the cylinders down to their several depths below the bed of the river, pontoons specially designed for the purpose were used. They were constructed with two apertures in them, of sufficient size to admit of the pair of cylinders passing through them at their proper distance from each other; and were also provided with four cylindrical legs capable of being lowered down to the bed of the river or lifted off it by hydraulic power. During the greater part of the time that cylinder sinking was going on four of these pontoons were employed, the dimensions of the largest being 80ft. x 67ft. x 7ft. deep. The work of cylinder sinking was carried out as follows:—A pontoon having been floated into position and its four legs lowered down to the bed of the river, the two cylinders for the pier were suspended in the apertures; and after having been lined with brickwork were gradually lowered down to the bed of the river by means of hydraulic jacks. The excavation for the cylinders was then proceeded with by means of a subaqueous digger worked by a crane on the pontoon. Owing to the nature of the strata through which the cylinders passed, it was necessary to weight them in order to force them down as the excavation proceeded; in some cases as much as 400 tons were placed upon the cylinder for this purpose. Where silty sand was met with, the use of a centrifugal pump was found to be of great assistance; the continual pumping of the water from inside the cylinder caused the sand beneath the cutting edge to be scoured towards the centre of the cylinder, where it could be more readily got at by the digger. When sunk to their required depths, the cylinders were filled with concrete; and the pontoon was then floated away to the next pier.

Depths of foundations.—The depths of the foundations vary from 6ft. to 38 1/2 ft. below the river bed as the average for the pair of cylinders. The shallowest foundations are at piers 7 and 8, where the cylinders rest on red sandstone; and the deepest at pier 20, which is founded on sandy clay. Thirty-three of the piers, including those for the thirteen large spans, rest on sand foundations;

¹ Paper read before the Institution of Mechanical Engineers, Edinburgh.

nd the average depth to which these cylinders are sunk below the river bed is 26½ft.

Testing of foundations.—All the foundations of the cylinder piers have been subjected to a weight 33 per cent. heavier than that which they will be required to carry.

Girders.—Including the wrought iron arches near the north end, there are eighty-one girder spans. The following are the lengths of the girders, taking them in the order in which they are placed in the viaduct from south to north :—

Table with 3 columns: No. of spans, Length of girders, and specific girder details. Includes rows for South end, High girders (13 spans), and North end.

From piers 4 to 28, 41 to 78, and 80 to 84, each span consists of four lattice girders with top and bottom members parallel, the roadway being carried on the upper members.

Transferring girders from old to new viaduct.—In the four-girder spans the first operation, after completing the piers, was to transfer the girders from the old to the new viaduct.

Floating out the high girders.—The work of floating out the girders for the thirteen large spans near the centre of the river, and of lifting them to the tops of the piers, was still more interesting.

Lifting the high girders.—The girders having been placed on the piers at this level, the next proceeding was to erect round and over their end posts the wrought iron pier superstructures.

Decking.—The decking or flooring is of the ridge and trough type. In the case of the high girders, where there are only two girders to the span, it is constructed with plates and channels.

Expansion.—The allowance for expansion is divided over thirty-two different places in the whole length, the sum of the calculated allowances amounting to 3ft. 8in.

Parapets.—The parapets or wind screens are of lattice work,

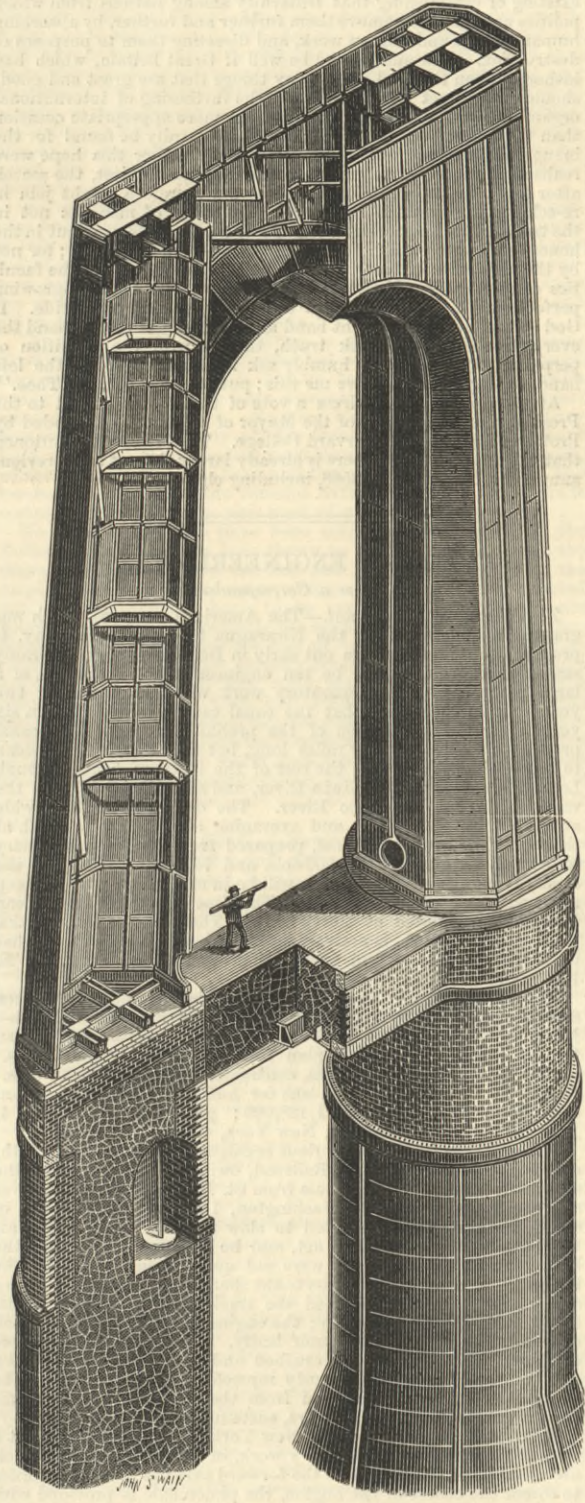
made of 3 x 5½in. bars, with standards about every 16ft., and finished off at the top with an oak coping.

Permanent way.—The permanent way is laid with cross sleepers, which are bedded in ballast in the troughs of the flooring.

Materials.—The various materials used in the construction were subjected to frequent testing throughout the work.

Wind pressure.—The calculations for wind pressure are based on a pressure of 56 lb. per square foot; and in estimating the area

Table listing materials used: Wrought iron in girders and piers (19,337 tons), Steel in flooring (3,540 tons), Cast iron (2,470 tons), Concrete (cement) (37,000 cub. yds.), Brickwork (25,700 tons).



SECTION OF PIER.

exposed to the wind, the bevelled ends of the piers are considered as flat surfaces, the wind screen as a solid surface, and 50 per cent. is added to the area of the outside girders.

Testing of Viaduct.—The viaduct has recently been subjected to very severe tests by the Board of Trade inspectors, the result being highly satisfactory.

Time occupied in construction.—The construction of the viaduct was commenced on June 22nd, 1882, and it was opened for passenger traffic on 20th June in the present year.

STATISTICS OF THE PRODUCTION OF PIG IRON.—The statistical report of the British Iron Trade Association has just been issued. The result may be thus summarised:—The stock of pig iron-makers' stocks in Scotland not included, being unknown—on December 31st, 1886, was 2,491,506 tons.

THE BRITISH ASSOCIATION.

SIR H. ROSCOE'S ADDRESS.

THE fifty-seventh annual meeting of the British Association was opened on Wednesday evening at Manchester by an address from the president, Sir H. E. Roscoe, M.P.

The President, in his inaugural address, said Manchester, distinguished as the birthplace of two of the greatest discoveries of modern science, welcomed the visit of the British Association for the third time. Those discoveries were the atomic theory of which John Dalton was the author, and the most far-reaching scientific principle of modern times—namely, that of the conservation of energy, which was given to the world about the year 1842 by Dr. Joule.

- 11,626. COMBINED CANE and UMBRELLA, W. P. Thompson.—(C. E. Vail, United States.)
- 11,627. GENERATING STEAM, J. F. Walker, Farnham.
27th August, 1887.
- 11,628. GENERATING SECONDARY STEAM, C. Howe and B. and J. H. Beckwith, London.
- 11,629. DOUBLE-CUFF GLOVE, H. Caston, London.
- 11,630. STOPPING LOOMS, F. T. Schmidt, Bradford.
- 11,631. GOVERNOR FOR ENGINES, W. F. Bowen, Bolton.
- 11,632. EXPANSIVE VESSELS OF STEAM TRAPS, A. Bradshaw, Accrington.
- 11,633. WASHING MACHINES, J. C. Balmforth and H. Hutchinson, Nottingham.
- 11,634. MEDALS OF CARDBOARD, &c., W. H. Watts, Birmingham.
- 11,635. WINDING MACHINES, W. and L. Tolson and J. Adams, Halifax.
- 11,636. ATMOSPHERIC INJECTOR, R. Robson, Leeds.
- 11,637. BICYCLES, &c., W. H. S. Aubin, Bloxwich.
- 11,638. INTERNALLY-STOPPERED BOTTLES, D. Rylands, Barnsley.
- 11,639. LOADING and UNLOADING COAL, W. E. Kochs, Cardiff.
- 11,640. KINDERGARTEN SPELLING-BOX, C. Hossfeld, London.
- 11,641. BOILERS, J. Peake, Manchester.
- 11,642. BEER PUMPS, S. Smith, Sheffield.
- 11,643. SHOOTING GAME, J. Hope, Liverpool.
- 11,644. SELF-CLOSING BALL VALVES, J. S. Walford, Birmingham.
- 11,645. STORING and AUTOMATIC SUPPLY OF OIL FOR LAMPS, C. W. Clarkson and F. Burnard, Newport.
- 11,646. ISSUING and REGISTERING APPARATUS, D. R. O'Sullivan, London.
- 11,647. RESPIRATOR and INHALER, S. F. Smith, London.
- 11,648. FARING, &c., VEGETABLES and FRUIT, D. Clan-Alpine Thatcher, London.
- 11,649. SHOP-WINDOW STANDS OF BRACKETS, A. C. Marlow, Worcestershire.
- 11,650. COMPOUND DONKEY PUMPS, S. C. Hattis, London.
- 11,651. BOXES OF CASES, A. Hood, Glasgow.
- 11,652. HYDRAULIC MOTORS, W. Fletcher, London.
- 11,653. CAUSTIC SODA and POTASH, F. P. E. de Lelande, London.
- 11,654. PERMANENT CRAMP BOTTLE STOPPER, S. H. Musgrave, Acton.
- 11,655. DOUBLE-GROOVED NECK GLASS BOTTLE, S. H. Musgrave, Acton.
- 11,656. STEERING GEAR, J. Robinson, London.
- 11,657. STOPPERS FOR BOTTLES, &c., J. Hands, London.
- 11,658. EXPLOSIVES, E. Edwards.—(R. Sjoberg, Sweden.)
- 11,659. REVOLVING RUBBER, L. Gillon, France.
- 11,660. Re-numbered 9256A.
- 11,661. BUNG BUSHES and VALVES, W. P. Thompson.—(M. Duhr, Prussia.)
- 11,662. SIEVING APPARATUS, P. van Gelder, Liverpool.
- 11,663. FASTENERS FOR SCARVES, &c., A. J. Boulton—(A. Lövy, Austria.)
- 11,664. COLOURING or STAINING WOOD, J. Munier and N. Salvaire, London.
- 11,665. MACHINE for DRYING WOOL, W. Nelson and E. Bowen, London.
- 11,666. METALLIC PLATES OF PLATING, S. Robertson, Glasgow.
- 11,667. EXTINGUISHING FIRE, H. Christie, London.
- 11,668. BALLING MACHINE, W. B. Lee, Bradford.
- 11,669. GAS LAMPS, H. W. and A. F. Cole, Stourport.
- 11,670. STEAM ENGINES, W. G. Strype, London.
- 11,671. WINDOW FASTENERS, G. H. and A. A. E. Needham, London.
- 11,672. VOLATILISATION of LEAD, &c., M. M. Bair, London.
- 11,673. SWAGING and WELDING the ENDS of WROUGHT METAL TUBES, &c., J. P. and E. S. T. Kennedy, London.
- 11,674. SUSPENDING, &c., ELECTRIC LAMPS, M. Bailey and J. Warner, London.
- 11,675. Re-numbered 4135A.

29th August, 1887.

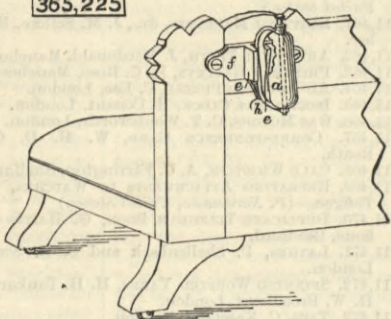
- 11,676. STAND PIPES for FIRE-EXTINGUISHING, J. W. Hearfield, Hull.
- 11,677. WARP MACHINES, A. Paget, Loughborough.
- 11,678. MINCING MACHINE and GAS MOTOR ENGINE, G. McGhee and P. Burt, Glasgow.
- 11,679. ANCHORS, W. P. Strawson, Birmingham.
- 11,680. COUPLING, &c., SHOP SHUTTERS, DOORS, &c., E. Jones, London.
- 11,681. BRUSH, W. H. Sellwood, London.
- 11,682. SELF-ACTING MULES, W. Dyson and T. Fisher, Halifax.
- 11,683. PACKING for CYLINDERS, &c., J. Taylor, Manchester.
- 11,684. SAFETY RIDING STIRRUPS, J. Harrison, Stamford.
- 11,685. LAND TILLING MACHINE, W. Gordon, Cullin.
- 11,686. ATTACHMENT of DOOR KNOBS to their SPINDLES, J. Tomkys, Codsall.
- 11,687. LACE and FABRICS on TWIST LACE MACHINERY, W. Gadd, Manchester.
- 11,688. REEL to HOLD SEWING COTTON, &c., R. Wright, Redditch.
- 11,689. TREATMENT of OIL or TAR obtained from BLAST FURNACES, A. H. Allen and R. Angus, Sheffield.
- 11,690. BALL and WHEEL CASTOR FRAM, J. Cheshire, Birmingham.
- 11,691. ARTIFICIAL SUPPORTS for SPINAL WEAKNESS, D. Kennedy, Glasgow.
- 11,692. CONVEYING PURE AIR into CITIES, &c., H. D. Child, London.
- 11,693. FIXING BEADS upon a FOUNDATION THREAD, G. Stein, London.
- 11,694. ROCKING CHAIR and HORSES, J. Simpson and S. T. Fawcett, London.
- 11,695. EXTRACTING JOINT PINS, &c., J. J. Hayhurst, St. Leonard's-on-Sea.
- 11,696. TAKING MEASUREMENTS, &c., for GARMENTS, J. Couteau, London.
- 11,697. COVERS to VESSELS for PRESERVING PERISHABLE ARTICLES, S. R. Stevenson, London.
- 11,698. GAS LAMPS, E. Stein.—(T. Gordon, United States.)
- 11,699. VALVES for LIQUID METERS, C. C. Barton, London.
- 11,700. PUMP or as a MOTOR ENGINE, G. de Mont-richard, London.
- 11,701. BURNING GAS for COOKING and HEATING PURPOSES, Q. S. Backus, London.
- 11,702. WIRE ROPES, H. R. I. Webster, London.
- 11,703. SAFETY FASTENERS for WINDOW SHAVES, A. Rose and R. Hunter, Glasgow.
- 11,704. INSULATORS, W. E. Langdon, J. C. and G. Fuller, London.
- 11,705. ELECTRIC LAMPS, E. B. Buty and E. Böhm, London.
- 11,706. CANS of JARS for LIQUID BLACKING, &c., H. J. Allison.—(S. M. Bibby, United States.)
- 11,707. WIND GAUGE SIGHT for FIRE-ARMS, H. J. Allison.—(W. Lyman, United States.)
- 11,708. HORIZONTAL BILL or LETTER FILE, F. Planner, London.
- 11,709. METAL CANS of CASES, J. A. Lloyd, London.
- 11,710. SPRING SADDLE for HOBBY HORSES, J. H. Howson, Sheffield.
- 11,711. ACTUATING BRAKES on BASSINETTES, &c., R. Ashton, Manchester.
- 11,712. WATCHES, H. Hammarlund, London.
- 11,713. RADIATORS, B. Russell, London.
- 11,714. CONNECTING CARRIAGE LAMPS to LAMP IRONS, H. Rogers, W. Howes, W. Burley, and W. Howes, London.
- 11,715. MACHINES for MINCING MEAT, &c., F. J. Gardner, London.
- 11,716. ENRICHING PITCH, M. L. Hobbay, London.
- 11,717. GAS MOTOR ENGINE, D. Embleton, London.
- 11,718. ACTUATING MECHANISM for ELECTROSTATIC GENERATORS, H. Gläser, London.
- 11,719. WATER CIRCULATING, &c., APPARATUS, &c., R. Fraser, Liverpool.

- 11,720. SAFETY LOCKING DEVICES, A. B. Pickard, London.
- 11,721. ROLLING TEA LEAF, W. Jackson, London.
- 11,722. TELEPHONE APPARATUS, J. Stewart.—(J. Hattinet, France.)
- 11,723. REGISTERING AUTOMATICALLY the NUMBER of ARTICLES WEIGHED by a WEIGHING MACHINE, P. G. Shadbolt, London.
- 11,724. MAGAZINE REPEATING FIRE-ARMS, F. Passler and F. Seidl, London.
- 11,725. BLANK AMMUNITION, P. Thaine.—(T. Norden-jelt, Sweden.)
- 11,726. SEALED LOCK and LABEL-CASE COMBINED, J. Verney, Wolverton.

SELECTED AMERICAN PATENTS.
(From the United States Patent Office Official Gazette.)

365,225. WALL-PROTECTING ATTACHMENT FOR FURNITURE, Frederick Barrows, Haverhill, Mass.—Filed April 6th, 1887.
Claim.—(1) As a new article of manufacture, a device of the character described, consisting of a bracket carry-

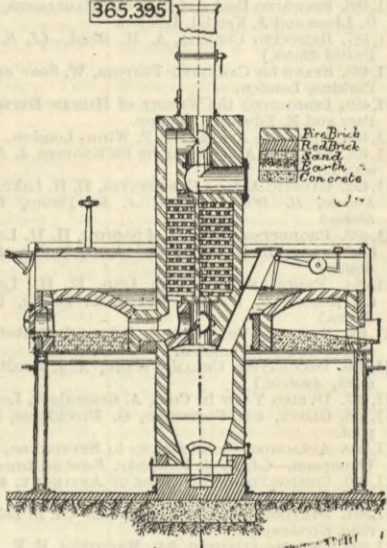
365,225



ing a roller and a spring, the latter being arranged to maintain the roller in the vertical plane, essentially as specified. (2) As a new article of manufacture, an attachment for sofas and other articles of furniture, consisting of a roller mounted in a supporting arm, and a bracket in which the said supporting arm is pivoted, substantially as described. (3) The combination, with a bracket *f*, and the pivoted arm *c*, carrying a roller *a*, of a spring *h*, at the back of said supporting arm, substantially as described. (4) The combination, with the bracket *f*, formed with lugs *e* of an arm *c*, pivoted between said lugs and carrying a roller *a*, and a spring *h*, secured to the bracket *f* between the lugs *e*, substantially as described.

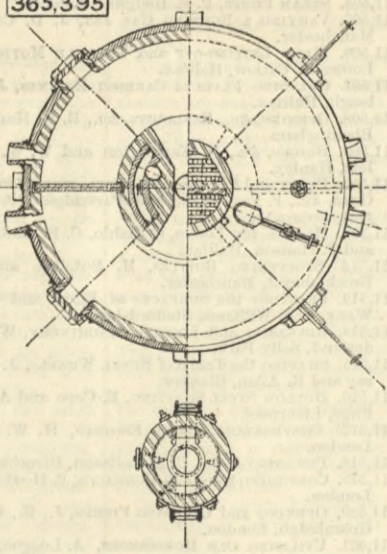
365,395. GAS FURNACE, H. W. Loss, Edge Moor, Del.—Filed June 7th, 1886.
Claim.—A continuous hearth of a circular, elliptical, or polygonal outline with two removable partition

365,395



doors, combined with and surrounding an inner independent structure consisting of an upper partition regenerator with a reversible valve and a lower gas

365,395



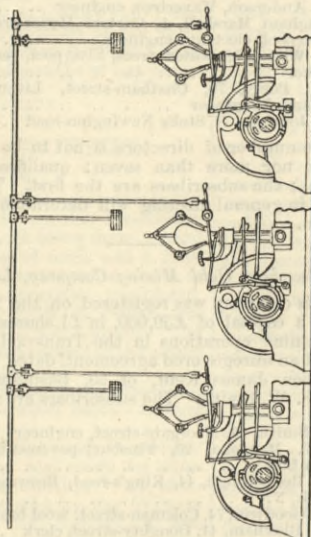
producer with a similar valve, the inner structure being connected with the outer hearth by two diametrically opposite situated openings or throats, substantially as and for the purpose specified.

365,465. VALVE GEAR, T. A. Edison, Menlo Park, N.J.—Filed October 12th, 1882.

Claim.—(1) The combination, with two or more engines having centrifugal governors, of connections between such governors causing them to act in unison, substantially as set forth. (2) The combination, with two or more steam engines, each operating one or more dynamo or magneto-electric machines, all of such machines being connected with the same conductors or systems of conductors, of a line or lines of connected shafting, and connections from said shafting to the throttle valve or cut-off mechanism of each engine,

whereby variations in such mechanism in one engine are both or all the other engines, substantially as set forth. (3) The combination, with the throttle valve or cut-off mechanisms of two or more engines and the line or lines of connected shafting, of removable and adjustable connections between them, substantially as set forth. (4) The combination of the valve or cut-off mechanisms of two or more engines, the line or lines

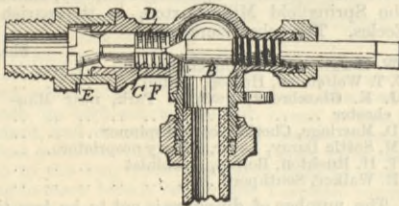
365,465



of connected shafting, connections between such mechanisms and such shafting, and means for holding such shafting in any position to which it is moved, substantially as set forth. (5) The combination of two or more steam engines, one or more dynamo or magneto-electric machines driven by each of said engines, all such machines being connected in multiple arc, and means for regulating the speed of both or all said engines simultaneously, substantially as set forth.

365,475. AUTOMATIC WATER-GAUGE VALVE, J. Kayser, New York, N.Y.—Filed February 3rd, 1886.
Claim.—(1) The combination of the automatic check valve E, the valve F, the pin D, and the spring C, whereby the closing of the valve F automatically opens the valve E, while the opening of the

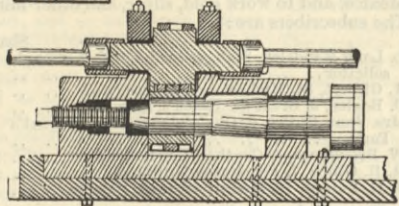
365,475



valve F does not close the valve E, substantially as described. (2) In an automatic gauge-cock, the combination of the valve E and its seat F with the screw-stem B, having the pin D and the spring C surrounding the spring D and bearing against the outer portion of the valve E, substantially as described.

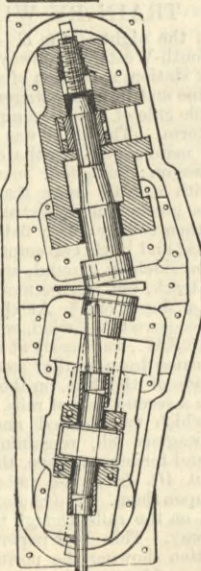
365,482. PROCESS OF ROLLING DAMASKEENED RODS, R. Mannesmann, Renscheid, Prussia, Germany.—Filed January 31st, 1885.
Claim.—(1) The process of forming damaskeened rods, which consists in passing a block or billet

365,482



formed of metals differing in quality or kind between rolls, and thereby reducing the size of the block simultaneously with imparting a spiral twist to the fibres of the metal, substantially as set forth. (2) The

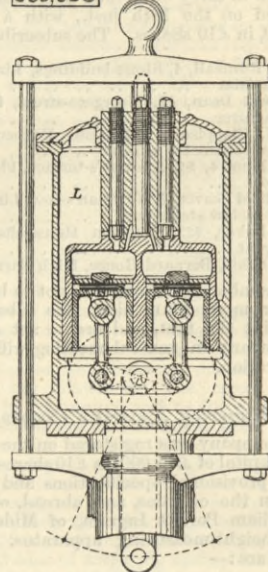
365,482



process of forming damaskeened rods, which consists in rolling a block or billet composed of metals differing in quality or kind through between rolls, so as to reduce the size and impart a spiral twist to the fibres, then uniting several of these rods and passing them again through rolls, so as to produce a rope-like inter-twisting of the fibres, substantially as set forth.

365,508. ENGINE GOVERNOR, G. E. Dow, San Francisco, Cal.—Filed September 7th, 1886.
Claim.—(1) A governor consisting of a cylinder containing liquid, a main piston moving vertically therein and connected with the supply valve of the engine, and the smaller alternately reciprocating pistons operating in corresponding chambers in the main piston, in combination with the upwardly-opening outlet valves in said pistons and the escape-passages through the main piston, substantially as herein

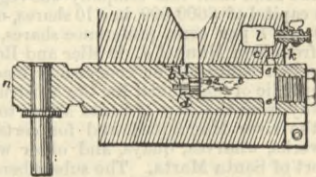
365,508



described. In a governor, a cylinder or chamber containing liquid, a piston fitting therein and connected with the supply valve of the engine, and smaller alternately reciprocating pistons operating in corresponding chambers in the main piston, and by which means the reactive force of the governor is sustained and controlled, in combination with the inlet valve K and passage L, communicating with the reservoir-space L and return passage W, substantially as herein described.

365,701. GAS-MOTOR ENGINE, N. A. Otto, Deuts-on-the-Rhine, Germany.—Filed February 17th, 1887.
Claim.—(1) Igniting apparatus for gas-motor engines, consisting of a slide *n* having a channel *b* communicating by a small hole *c* with a chamber *d* that in its turn communicates by an annular opening *d* with a passage

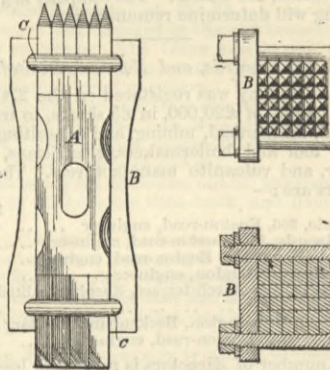
365,701



e having opposite lateral openings *e* ¹ ², the passage *e* being made to communicate with the firing port of the engine by a passage *h*, substantially as described. (2) In combination with the passage *e* ¹ ² of the igniting slide *n*, the chamber *l*, communicating with the outer air by a regulating cock *g*, and with the said passage by an opening *k*, substantially as herein described.

365,707. STONE-DRESSING HAMMER, J. S. Squires, Jordan.—Filed December 4th, 1885.
Claim.—The combination of the head or body A, the plate B, secured to said body on one side, removable

365,707

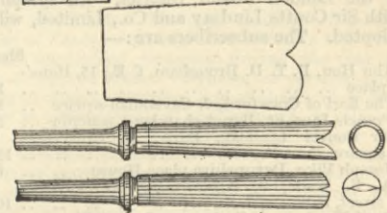


points or chisels supported by the body-plate, and the stirrup clamps C C, clamping said points or chisels and secured in holes formed in the plate near its ends substantially as described.

365,819. ART OF WELDING THE ENDS OF METAL TUBES, H. Jordan, Northampton, Mass.—Filed April 23rd, 1886.

Claim.—The improved art herein described of butt-welding the ends of metal tubes, consisting in first shaping the end to be welded, then closing the end of

365,819



the tube sufficiently to bring the edges each opposite to the other, and then heating and welding between dies shaped to force the inwardly-bent portions of the end of the tube together and form a butt-weld, substantially as and for the purpose set forth.

RAILWAY EXTENSION IN CEYLON.—In his first report on the Uva Province, issued by Government, Mr. Kirg urges that a decision should be come to very soon as regards the extension of the railway by some route and on some gauge. Ceylon people were glad to learn by last mail from Mr. T. N. Christie, the chairman of the Ceylon Planters' Association, that on the day after the mail left England he was to have an interview with Sir Henry Holland on this subject, and they hoped that at length the extension would be sanctioned.